



Surface Water Management Plan

Cherry Orchard Point – Proposed Development at Sites 4 and 5, Park West Avenue, Dublin 10

October 2023

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This document has been prepared and checked in accordance with Waterman Group's IMS (BS EN ISO 9001: 2015 and BS EN ISO 14001: 2015)

| Issue | Date | Prepared by | Checked by | Approved by |
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Comments



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A. GDSDS Attenuation Calculations

1. Introduction

1.1 Context

This report has been prepared by Waterman Moylan Consulting Engineers, on behalf of the LDA for a proposed development at Sites 4 and 5, Park West Avenue, Dublin 10.

The report sets out to demonstrate how pollution of watercourses both during the construction stage and after the construction period, during the operational stage will be prevented and/or mitigated. This is in accordance with SI25 of the DCC Development Plan 2022-28, which requires "*the preparation of a Surface Water management Plan as part of all new developments in accordance with the requirements of Appendix 13 – The Council's Surface Water Management Guidance.*". This is required for 2 or more residential units or commercial space of 100m² or greater, both of which are appliable to the proposed development. Appendix 13 advises that the following items are to be included in a Surface Water Management Plan, and in brackets which section of this report they are discussed:

- Site location map with proposed planning boundary indicated in red. (Figure 1)
- Overall surface water drainage layout indicating:
 - Existing public surface water infrastructure. (Section 4.2)
 - Proposed connection points to existing public sewers. (Section 4.2)
 - Spine sewers, if any. (Sections 1.6 & 4.2)
 - Detail of any surface water sewer extension, diversions, surface water sewer upgrades etc. to be clearly indicated. (None proposed)
- Report detailing existing site conditions including:
 - Topography. (Section 1.3)
 - Ground conditions. (Section 1.4)
 - Land drain features. (None proposed)
 - Overland flow paths. (Section 4.4.3)
 - Floodplains. (Section 4.4.3)
 - Utilities. (Section 4.5)
- Detail of proposed surface water management strategy shall include:
 - Longitudinal section details of proposed surface water pipe runs if required indicating route, levels, pipe size, gradient etc. A well-designed SuDS scheme will reduce or even eliminate the need for significant piped drainage. Surface Water Management Guidance | Appendix 13 358. (Section 4.5)
 - Identify proposed location to discharge to stream or public drainage system. (Section 4.2)
 - Identification of appropriate SuDS features to meet the key criteria of the GDSDS and reference in Section 16.3 of the Greater Dublin Regional Code of Practice for Drainage Works - source control and interception storage provided and volumes defined – no run-

off from site for events up to 5mm. See also the Council's Sustainable Drainage Design & Evaluation Guide (2021) and Appendix 12. (Sections 4.4 to 4.4.4)

- Provide a clear explanation of the SuDS proposals proposed for each hardstanding area including defined control structures and sizes of same. (Sections 4.4 to 4.4.4)
- Discharge rate applied. (Section 4.2)
- Attenuation storage provided and volumes defined storage for 1% and 3.3% annual probability with factor in accordance with the SFRA for climate change shall be applied. A figure of 20% will be applicable in most cases. (Section 4.4)
- Exceedance and overland flow routes. (Section 4.4.3)
- Phased development where development under a planning application/permission is phased, coordination of the overall surface water management strategy shall be implemented at the first phase in order to ensure the overall integrated design is implemented. This would allow different parts of a site to be developed at different times, while ensuring that the final developed site shall meet the overall design criteria as set out in this Appendix. (Sections 1.5 & 1.6)
- Identify green space and public space locations including any that are designed to be multifunctional – integrating SuDS (see also Section 15.6 – Green Infrastructure and Landscaping). (Section 1.5)
- Details of any proposed wayleaves or land transfers in relation to surface water drainage. (Not applicable)
- An undertaking that SuDS will be completed to taking in charge standards (in accordance with Policy SI26). (Section 4.5)

1.2 Site Location and Description

The subject masterplan development is comprised of 2 No. sites. Site 4 & Site 5 are bisected by Park West Avenue and lie to the west and east of this roadway respectively, as per the blue boundary lines indicated on *Figure 1* overleaf.

The Site Investigation Report undertaken by Ground Investigations Ireland (GII) is included as an appendix to the Preliminary Construction Environmental Management Plan, submitted under a separate cover, determined that Site 4 is combination of Greenfield and Brownfield, with evidence of fill material in the area of the site previously used as a construction compound. Site 5 is predominantly a brownfield site, with fill material found for the same reason.

Site 4 is bound to the west by the M50, to the south by the Dublin-Kildare rail line and the Park West & Cherry Orchard station, and to the east and north by Park West Avenue. Site 5 is bound to the west by Park West Avenue, the northwest by Cedar Brook Way, the northeast and east by Barnville Park, and to the south by the Dublin-Kildare rail line and the residential unit of 62 Barnville Park.

Site 4 is currently access via a secured gate from Park West Avenue. Site 5 is accessed via a similar arrangement from Cedar Brook Way.

The area of the subject application is indicated by the red boundary line, also on *Figure 1* overleaf. A letter of consent has been obtained for the area of public works required.

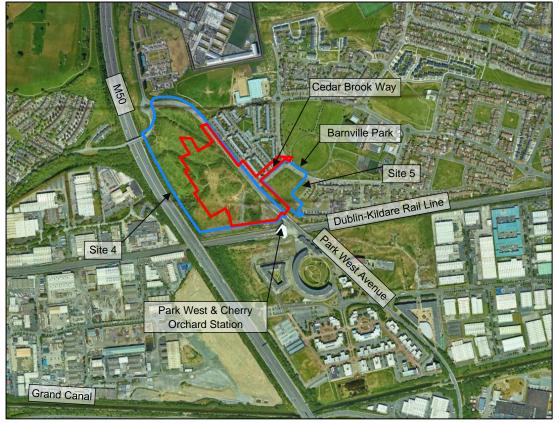


Figure 1 | Site Location (Source: Google Earth)

The overall masterplan development area as per the blue line boundaries is c. 13.02ha, with Site 4 being c. 11.41 ha and Site 5 being c. 1.61ha. The area of the subject application indicated by the redline boundary, including for works in the public domain, is 6.16ha (61,648m²).

The project archaeologist, Archer Heritage Planning Ltd., have identified the ploughed out remains of a Fulacht Fia located centrally on site 4, adjacent to the convergence of 2 No. static ditches on their southern side. The archaeologist has recommended that the remains of the Fulacht Fia be preserved by record prior to further works being undertaken on site.

1.3 Topographic details

For Site 4, the topographic survey of the area indicates that the low point of the site has a level of 55.72m OD. This is located on the eastern site boundary approximately 140m north of the junction of Park West Avenue and Cedar Brook Way. The remainder of the site generally slopes to this location owing to the embankments and subsequent site grading from the Dublin-Kildare Rail line to the south, M50 to the west, and approach road to the overpass on the M50 to the north.

Site 5 has a central high point with a level of 58.05m OD, and slopes outwards to all boundaries. The boundaries of Site 5 typically have levels between 54.80m and 56.00m, with the higher of these levels being

located to the south of the site, adjacent to the retaining wall of the Park West Avenue Bridge over the rail lines.

Ordnance survey and topographic survey mapping indicates that Site 4 contains static ditches with no outfall. These ditches previously had hydrological connectivity and flow, which has been cut-off by the construction of the M50 to the east and the Cedar Brook housing development to the west, as discussed in Chapter 11 of the EIAR report. These ditches normally remain dry except in heavy rainfall events where water that is not percolated via the site's naturally grassed landscaping, would collect locally in these static ditches for infiltration to the groundwater table. Site 5 does not have any form of surface drainage network and conveys rainfall directly to the soils via its grassed landscape. There is potential during heavy rainfall events, that the ground may become saturated and unable to further infiltrate rainfall, which would then run from the surface, over the boundary and to the adjacent road networks to outfall to the storm drainage networks serving these roads. The sites are located in the catchment of the Blackditch stream, a tributary of the Camac River which has an ultimate outfall to the River Liffey at Heuston Station.

1.4 Site Investigation Details

Site investigations for both sites were undertaken in 2022 by Ground Investigations Ireland (GII), the technical Ground Investigation report was completed in November 2022, and the Waste Analysis Classification report was completed in October 2022. Both these reports are included as appendices to the Construction Environmental Management Plan, submitted under a separate cover.

The fieldworks comprised a programme of 14 no. trial pits with dynamic probes, and 11 No. soakaway tests. 14 No. Cable percussion and 19 No. rotary boreholes, 3 No. groundwater monitoring and geotechnical and environmental laboratory testing was also undertaken. The locations are indicated in *Figure 2*. The procedures undertaken as part of the site investigation were in accordance with Eurocode 7 Part 2: Ground investigation and testing (ISEN 1997-2:2007) & B.S. 5930:2015.

Trial pits were excavated using an 8.5T tracked excavator at the locations indicated in *Figure 2*. The locations were checked using a CAT scan to minimise the potential for encountering services during the excavation. The Trial Pits were sampled, logged, and photographed by a Geotechnical Engineer/Engineering Geologist prior to backfilling with arisings. Notes were made of any services, inclusions, pit stability, ground water encountered, and the characteristics of the strata encountered and are presented on the trial pit logs, which are provided in Appendix 2 of the Site Investigation report. The site investigation report is included in full as an appendix to the Preliminary Construction Environmental Management Plan report, submitted under a separate cover.

The soakaway testing was carried out in selected trial pits at the locations indicated in *Figure 2*. These pits were carefully excavated and filled with water to assess the infiltration characteristics of the proposed site. The pits were allowed to drain and the drop in water level was record over time as required by BRE digest 365. The pits were logged prior to completing the soakaway test and were backfilled with arisings upon completion. The results are included as an appendix to the Site Investigation report.

The dynamic probe tests (DPH) were carried out at the locations shown in *Figure 2*, in accordance with B.S. 1377: Part 9 1990. The test consists of mechanically driving a cone with a 50KG weight in 100mm intervals and monitoring of the number of blows required. An equivalent standard Penetration test (SPT)

"n" value may be calculated by dividing the total number of blows over a 300mm drive length by 1.5. The dynamic probe logs are provided as an appendix to the Site Investigation report.

The cable percussion boreholes were drilled using a Dando 2000 drilling rig with regular in-situ testing and sampling undertaken to facilitate the production of geotechnical logs and laboratory testing. The standard method of boring in soil for site investigation is known as the Cable Percussion method. It consists of using a shell in non-cohesive soils and a clay cutter in cohesive soils, both operated on a wire cable. Very hard soils, boulders, and other hard obstructions are broken up by chiselling and the fragments removed with the shell. Where ground conditions made it necessary, the borehole was lined with 200mm diameter steel casing. While the use of the cable percussion method of boring gives the maximum data on soil conditions, some mixing of laminated soil is inevitable. For this reason, thin lenses of granular material may not be noticed. Disturbed samples were taken from the boring tool at suitable depths, so that there is a representative sample at the top of each change in stratum and thereafter at regular intervals down the borehole until the next stratum was encountered. The disturbed samples were then sealed and sent to the laboratory where they were visually examined to confirm the description of the relevant strata. Standard penetration tests were carried out in the boreholes. The results of these tests, together with the depths at which the tests were taken, are shown on the accompanying borehole records in the Site Investigation report. The test consists of a thick wall sampler tube, 50mm external dia., being driven into the soil by a Hammer/Weight weighing 63.5kg and with a free drop of 760mm. For gravels and glacial till the driving shoe was replaced by a solid 60° cone. The standard penetration test number referred to as the "n" value is the number of blows required to drive the tube 300mm, after an initial penetration of 150mm. The number gives a guide to the consistency of the soil and can be used to estimate the relative strength/density at the depth of the test and also to estimate the bearing capacity and compressibility of the soil. The cable percussion borehole logs are provided in Appendix 5 of the Site Investigation report.

The rotary coring was carried out by a track mounted T44 Beretta rig at the locations shown in Figure 2. The rotary boreholes were complete from the ground surface or alternatively, where noted on the individual borehole log, from the case of the cable percussion borehole where a temporary liner was installed to facilitate follow-on rotary coring. The T44 Beretta is equipped with rubber tracks which allow for short travel on pavement surfaces avoiding any damage of the surface. The T44 Beretta utilises a triple tube core barrel system operated using a wireline drilling process. The outer barrel is rotated by the drill rods and at its lower end, carries the coring bit. The inner barrel is mounted on a swivel so that it does not rotate during the process. The third barrel or liner is placed within the second one to retain the core intact and to preserve as much as possible the fabric of the drilling stratum. The core is cut by the coring bit and passes to the inner liner. The core is brought up to the surface within the inner barrel on a small dia. wire rope or line attached to the "overshoot" recovery tool which is then placed into a core box in order of recovery. A drilling fluid, typically air mist or water flush is passed from the surface through hollow drill rods to the drill bit and is used to cool the drill bit. Temporary casing is used in some situations to support unstable ground or to seal off fissures or voids. It should be noted that the rotary coring can only achieve limited recovery in overburden, particularly granular or weakly cemented strata due to the flushing medium washing away the cohesive fraction during coring, The recovery achieved, where required is noted on the borehole logs and core photographs are provided to allow assessment of the core recovered. The rotary borehole logs are provided in Appendix 5 of the Site Investigation report.

Groundwater monitoring installations were installed upon the completion of selected boreholes to enable sampling and the determination of the equilibrium groundwater level. The typical groundwater monitoring

installation consist of a 50mm uPVC/HDPE slotted pipe with a pea gravel response zone and bentonite seal installed to the engineer's specification. Where required the standpipe is sealed with a gas tap and finished with a durable steel cover fixed in place with a concrete surround. The installation details are provided on the exploratory hole logs in the appendices of the Site Investigation report.

Samples were selected from the exploratory holes for a range of geotechnical and environmental testing to assist in the classification of soils and to provide information for the proposed design. Environmental and chemical testing as required by the specification, including the Rilta Suite, pH, and Sulphate testing was carried out by Element Materials Technology Laboratory in the UK. The Rilta Suite testing includes both solid waste and Leachate Waste Acceptance Criteria. Geotechnical testing consisting of moisture content, Atterberg limits, Particle Size Distribution (PSD), and hydrometer tests were carried out in Prosoils Geotechnical Laboratory in the UK. The results of the laboratory testing are included in the suite.



Figure 2 | Site Investigation Test Locations

1.5 Proposed Subject Development

The subject application is for Phase 1 of a 4-phase masterplan development as per Figure 3 overleaf.

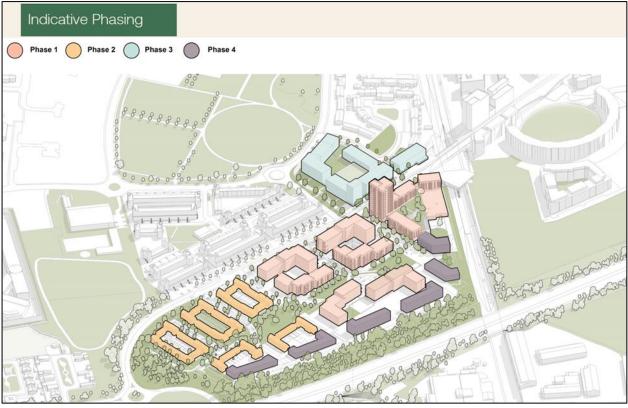


Figure 3 | Phasing Layout

Phase 1 is the medium and high-density area and the subject application area, which will provide a total of 708 residential units ranging in size from studio to 3-bed apartments, a 2,523m² supermarket, a combined area of 373m² for retail over 7 units, a 672m² creche and 1,222m² of community spaces over 13 buildings. A breakdown of the schedule of accommodation for the subject application is provided in *Table 1* overleaf.

| Block | Studio | 1-bed Apt | 2-bed Apt | 3-bed Apt | Total | Total Area |
|-------------|--------|-----------|-----------|-----------|-------|---------------------|
| 1 | - | 13 | - | 11 | 24 | - |
| 2A | - | 8 | 14 | 5 | 27 | - |
| 2B | 1 | 43 | 66 | - | 110 | - |
| 3 | - | 12 | 23 | - | 35 | - |
| 5A | 10 | 16 | 28 | - | 54 | - |
| 5B | - | 10 | 14 | 5 | 29 | - |
| 6A | - | 20 | 32 | 6 | 58 | - |
| 6B | - | 8 | 12 | 4 | 24 | - |
| 7A | 6 | 35 | 40 | - | 81 | - |
| 7B | - | 5 | 25 | - | 30 | - |
| 8A | 6 | 17 | 34 | 6 | 63 | - |
| 8B | 5 | 13 | 10 | 5 | 33 | - |
| 9A | - | 29 | 13 | 5 | 47 | - |
| 9B | - | 8 | 10 | 4 | 22 | - |
| 10A | - | 16 | 22 | 4 | 42 | - |
| 10B | - | 10 | 14 | 5 | 29 | - |
| Supermarket | | | | | 1 | 2,523m ² |
| Retail | | | | | 7 | 373m² |
| Community | | | | | 13 | 1,222m² |
| Creche | | | | | 1 | 672m² |

 Table 1 | Phase 1 Schedule of Accommodation

The development includes all associated site works, undergrounding of overhead lines, boundary treatments, drainage, and service connections.

1.6 Proposed Masterplan Development

The remainder of phases as per *Figure 3* will be subject to their own planning permission applications, however their preliminary details are outlined below so that the subject development may be assessed as part of the full masterplan development in its full context. It should be noted that the trunk foul and surface water drainage, including attenuation storage, to serve phases 2, 3, & 4 are part-provided under the subject application for Phase 1.

Phase 2: This is the low-density housing area located to the north of Site 4 and contains 153 residential units comprising 100 apartment/ duplex units and 53 houses.

Phase 3: This will be the development of Site 5, and comprises 254 residential units, 1,200m² of retail space, with community facilities to be confirmed.

Phase 4: This will be the construction of commercial office space over 6 blocks with a total area of c. 16,310m².

1.7 Surface Water Impacts

Surface water run-off from surface construction activities has the potential to become contaminated. The main contaminants arising from construction activities include:

- Suspended solids: arising from ground disturbance and excavation;
- Hydrocarbons: accidental spillage from construction plant and storage depots;
- Faecal coliforms: contamination from coliforms can arise if there is inadequate containment and treatment of onsite toilet and washing facilities; and
- Concrete/cementitious products: arising from construction materials.

These pollutants pose a temporary risk to surface water quality for the duration of the project if not properly contained and managed.

1.8 Proposed Construction Works

It is currently estimated that Phase 1 which is the subject application will commence end of 2024 with a 4year construction programme for completion by the end of 2028. The remainder of the masterplan lands, Phases 2, 3, & 4 as per *Figure 3*, are estimated to be completed by 2032.

Working hours for the site will be set out in the conditions of planning approval and would typically be 08.00 to 19.00 from Monday to Friday and 08.00 to 14.00 on Saturday. No Sunday or Bank Holiday work will generally be permitted. The above working hours are typical; however, special construction operations may need to be carried out outside these hours in order to minimise disruption to the surrounding area.

The proposed work will consist of the following:

- Site preparation;
- Erection of security fencing/perimeter fencing;
- Setting up a secure site compound including wash down area;
- Site clearance including topsoil stripping;

- Construction of infrastructure including roads, drainage, and services;
- Provision of road upgrades and pedestrian links;
- Construction of residential and commercial units.
- Reinstatement landscaping.

2. Mitigation Measures

The sites have no direct hydrological connectivity to natural watercourses or surface water networks. There may be an indirect link from surface water runoff which may have the potential to run off the site boundary to the surface water gullies on the adjacent road networks. These networks outfall to the Blackditch Stream.

The following Mitigation Measures are to address potential impacts to water quality and are required to protect the Blackditch Stream, and the Camac River which has an ultimate outfall to the River Liffey at Heuston. All works will be undertaken with reference to the following guidelines:

- CIRIA C532: Control of Water Pollution from Construction Sites, Guidance for Consultants and Contractors (Masters-Williams et al., 2001);
- CIRIA C692: Environmental Good Practice on Site, (Audus et al., 2010)
- BPGCS005: Oil Storage Guidelines;
- CIRIA C648: Control of Water Pollution from Linear Construction Projects: Technical Guidance (Murnane et al., 2006a)
- CIRIA C648: Control of Water Pollution from Linear Construction Projects: Site Guide (Murnane et al., 2006a)
- Guidelines on Protection of Fisheries During Construction Works in and Adjacent to Waters (IFI 2016)
- Guidelines for Planning Authorities Architectural Heritage Protection Guidance on Part IV of the Planning and Development Act 2000. (Part 2, Chapter 7) and ICOMOS Principles.

The schedule of mitigation presented within *Table 2* summarises measures that will be undertaken in order to reduce impacts on ecological receptors within the zone of influence of the proposed development.

| No. | Risk | Possible Impact | Mitigation | Result of Mitigation |
|-----|---|---|--|---|
| 1 | Hydrocarbons from carparking area entering the drainage network. | Water quality impacts. | Petrol interceptor to be installed on drainage network prior to outfall to public surface water network. | Prevents hydrocarbons from entering the public surface water network. |
| 2 | Pollutants from site compound areas entering the drainage network or contaminating soils. | Water quality impacts. Soil quality impacts. Groundwater impacts. | Materials to be stored appropriately in designated areas (discussed below). Temporary foul water connection to be obtained from Uisce Eireann to serve site compound welfare facilities. | Prevents contamination of public surface water network, soil, and groundwater. |

| No. | Risk | Possible Impact | Mitigation | Result of Mitigation |
|-----|---|---|--|---|
| | | | Fuels, oils, greases, and other potentially polluting chemicals will be stored in roofed and bunded compounds at the Contractor's compound. | |
| 3 | Pollutants from material storage areas entering the watercourse or contaminating | Water quality impacts. Soil quality impacts. Groundwater | Storage area to be located over 50m away to ensure no direct pathway to the surface water network. Bunds are to be provided with 110% capacity of storage container. | Prevents contamination of public surface water |
| | soils. | impacts. | Spill kits will be kept on site at all times and all staff trained in their appropriate use. | |
| | | | Method statements for dealing with accidental spillages will be provided the Contractor for review by the Employer's Representative. | |
| | Concrete/ cementitious | | A designated wash down area within the | Prevents contamination of public surface water network. |
| 4 | materials entering the drainage network.Water quality impactsContractor's compound will be used for cleaning of any equipment or plant, with the safe disposal of any contaminated water. | | Ensures invasive species material is not transported off site as muck. | |
| 5 | Leaching of contaminated soil into groundwater. | Groundwater quality impacts | Spill kits will contain 10 hr terrestrial oil booms (80mm diameter x 1000mm) and a plastic sheet, upon which contaminated soil can be placed to prevent leaching to ground water. | Prevents contamination of groundwater. |
| | Pollutants from equipment storage/ | | Any refuelling and maintenance of equipment will be done at designated bunded areas with full attendance of plant operative(s) within contained areas. | Prevents contamination |
| 6 | refuelling area entering the | Water quality impacts | Discharge licence (where required) pollutant limits to be monitored and adhered to. | of public surface water network. |
| | drainage network. | | The site is located at least 50m from any direct pathway to the surface water drainage network. | |
| 7 | Runoff from exposed work areas and excavated material storage areas entering the drainage network. | Water quality impacts due to silt entering the network. | Provision of silt entrapment facilities such as; straw bales, silt fencing, silt barriers, diversion drains, settlement tank(s), & settlement pond(s), as appropriate and as outlined below. | Prevents contamination of public surface water network. |

Table 2 | Schedule of Surface Water Mitigation Measures

3. Construction Stage

The proposed potential pollution mitigation measures outlined below will be implemented in accordance with 'CIRIA C532 – Control of Water Pollution from Construction Sites – Guidance for Consultants and Contractors' – CIRIA-2001.

3.1 Roles and Responsibilities

3.1.1 Main Contractor

The Main Contractor will have overall responsibility for the implementation of the project Construction Surface Water Management Plan (CSWMP) during the construction phase. The appointed person from the Main Contractors team will be appropriately trained and assigned the authority to instruct all site personnel to comply with the specific provisions of the CSWMP. At the operational level, a designated person from each sub-contractor on the site shall be assigned the direct responsibility to ensure that the operations stated in the CSWMP are performed on an on-going basis.

Copies of the Construction Surface Water Management Plan will be made available to all relevant personnel on site. All site personnel and sub-contractors will be instructed about the objectives of the CSWMP and informed of the responsibilities which fall upon them because of its provisions.

The responsibilities of the appointed person will be as follows;

- Updating the CSWMP as necessary to reflect activities on site.
- Advise site management (including, but not limited to, the site Construction Manager) on environmental matters.
- Ensure pre-construction checks for protected species, if any, are undertaken.
- Review method statement of the sub-contractors to ensure that it incorporates all aspects of CSWMP.
- Provide toolbox talks and other training, and ensure understanding by all involved of all mitigation measures.
- Assess effectiveness of mitigation, check weather forecast and site conditions where trigger levels are required.
- Ensure adherence to the specific measures listed in the Planning Conditions.
- Advise upon the production of written method statements and site environmental rules and on the arrangements to bring these to the attention of the workforce.
- Investigate incidents of significant, potential, or actual environmental damage, ensure corrective actions are carried out and recommend means to prevent recurrence; and,
- Be responsible for maintaining all environmental related documentation.
- Ensure plant suggested is environmentally suited to the task in hand.
- Co-ordinate environmental planning of the construction activities to comply with environmental authorities' requirements and with minimal risk to the environment. Give contractors precise

instructions as to their responsibility to ensure correct working methods where risk of environmental damage exists.

3.2 Pre-Construction Plan

3.2.1 Designated Storage Area & Site Compound

A site compound(s) including offices and welfare facilities will be set up by the main contractor in locations to be decided within the subject site.

The main contractor will be required to schedule delivery of materials daily. The main contractor will be required to provide a site compound on the site for the secure storage of materials.

Measures will be implemented throughout the construction stage to prevent contamination of the soil and surrounding watercourses from oil and petrol leakages and significant siltation. Suitable bunded areas will be installed for oil and petrol storage tanks. Designated fuel filling points will be put in place with appropriate oil and petrol interceptors to provide protection from accidental spills. Spill kits will be provided by the Contractor to cater for any other spills.

3.3 Construction Plan

3.3.1 Vehicle Washdown

Where possible, and subject to licence, the permanent connection to the public foul sewer will be used temporarily for construction phase. Vehicle wash down water will discharge directly, via suitable pollution control and attenuation, to the foul sewer system. If this connection is not permitted, then wastewater generated will be required to be stored for collection and treatment off-site at a suitable waste disposal facility.

3.3.2 Surface Water Run-off

On-site treatment measures will be installed to treat surface water run-off from the site prior to discharge to the receiving surface water sewer on Park West Avenue. This treatment will be achieved by the construction of settlement tanks/ponds, in conjunction with the installation of proprietary surface water treatment systems including class 1 full retention petrol interceptors, and spill protection control measures. Settlement tanks/ponds will be sized to deal with surface run-off and any groundwater encountered.

A sampling chamber with shut down valve will be installed downstream of the settlement pond/tank and water quality monitoring will be carried out here prior to discharge to the surface water sewer.

It is likely that the surface water run-off from the site will be discharged to the existing public surface water network, post treatment. This will need to be confirmed between the Contractor and Local Authority, as well as any further conditions such as the permitted levels of contamination as well as frequency for testing, as part of the Contractor's application for a discharge licence.

3.3.3 Surface Water Monitoring Parameters

In addition to daily visual inspections, a surface water monitoring programme, as outlined in *Table 3* must be followed during construction in order to ensure maintenance of water quality protection. This is in line

with Transport Infrastructure Ireland (TII)'s 'Guidelines for the Creation, Implementation and Maintenance of an Environmental Operating Plan'. It is considered that the parameter limit values (Guide/Mandatory) defined in the Fresh Water Quality Regulations (EU Directive 2006/44/EEC) should act as a trigger value for the monitoring of Surface Water.

| Deremeter | Limit | | Frequency and Manner of | |
|---------------------------|---|-----------------|--|--|
| Parameter | Limit Value | Guide/Mandatory | Samplings | |
| Temperature | 1.5°C | Mandatory Limit | Weekly, and at appropriate intervals where the works activities associated with the scheme have the potential to alter the temperature of the waters. | |
| Dissolved oxygen | 50% of Samples ≥ 9 (mg/l O2) 100% of Samples ≥ 7 (mg/l O2) | Guide Limit | Weekly, minimum one sample representative of flow oxygen conditions of the day of sampling | |
| рН | 6 to 9 | Mandatory Limit | Weekly | |
| Nitrites | ≤0.01 (mg/l N02) | Guide Limit | Monthly | |
| Suspended Solids | ≤25 (mg/l) | Guide Limit | Monthly | |
| BOD5 | ≤3 (mg/l) | Guide Limit | Monthly | |
| Phenolic Compounds | - | - | Monthly where the presence of phenolic compounds is presumed (An examination by test) | |
| Petroleum Hydrocarbons | 5 (mg/l) | Guide Limit | Monthly (visual) | |
| Non-Ionized Ammonia | ≤ 0.005 (mg/l NH3) | Guide Limit | Monthly | |
| Total Ammonium | ≤ 0.004 (mg/l NH4) | Guide Limit | Monthly | |
| Total Residual Chlorine | ≤ 0.005 (mg/l HOCl) | Mandatory Limit | At appropriate intervals where works activities associated with the scheme have the potential to alter the Total residual Chlorine of the waters | |
| Electrical Conductivity | - | - | Weekly | |

Table 3 | Monitoring Guidelines (Fresh Water Quality Regulations)

4. Operational Stage

The design of the surface water network is discussed in full in the Engineering Assessment Report, submitted under a separate cover. This report, however, discusses the surface water management plan as a whole, with an emphasis on describing the rational for the selection of proposed SuDS, and calculations for attenuation volumes, discharged water quality enhancement, and the further enhancement of amenity and biodiversity values. The following sections may be considered as the "SuDS Design statement" as required under Section 9.11 of the Council's SuDS Design & Evaluation Guide.

4.1 SuDS

The Council's SuDS Design & Evaluation Guide advises that: "Sustainable Drainage or SuDS is a way of managing rainfall that minimises the negative impacts on the quantity and quality or runoff while maximising the benefits of amenity and biodiversity for people and the environments.". These Sustainable Drainage System (SuDS) are considered a collection of water management practices that aim to align modern drainage systems with natural water processes.

Sustainable Drainage System (SuDS) are a collection of water management practices that aim to align modern drainage systems with natural water processes.

SuDS facilities are designed to prevent pollution of streams and rivers and to slow down runoff from sites, therefore helping to prevent downstream flooding and improve water quality. This closely mimics natural catchment behaviour where rainfall either infiltrates through the soil or runs off slowly over the ground surface to the nearest watercourse. This is known as the "treatment train" approach. SuDS devices should be placed at source, site, and regional levels. SuDS can also provide amenity benefits to local communities and benefits for biodiversity simultaneously.

Dublin City Council's Development Plan (2022-2028) has identified SuDS as the preferred method of managing rainfall from new developments. The proposed SuDS for the subject application have been incorporated and designed in accordance with Dublin City Council's SuDS Design and Evaluation Guide and also in accordance with their Green and Blue Roof Guide.

In the following sections of the it will be outlined in detail how SuDS devices have been utilised and incorporated as an integral part of the overall plan for the proposed development, and how their inclusion will mitigate the risk of localised and downstream flooding, while also promoting residential amenity and biodiversity.

The proposed SuDS measures have been assessed for suitability, designed, and incorporated in accordance with CIRIA Report C753 The SuDS Manual, and Dublin City Council's SuDS Design and Evaluation Guide, and Green & Blue Roof Guide, in order to develop a nature-based approach to surface water management for the proposed development.

4.2 Proposed Surface Water Network and SuDS Strategy

It is proposed to construct a stormwater drainage network that will service and attenuate the development internally before discharging at the current greenfield (or allowable) rates to the local Surface Water network. It is proposed that Site 4 will connect to the existing 1,050mm Ø network in Cedar Brook Way, while Site 5 will outfall to the 900mm Ø Network in Barnville Park.

Based on the details presented by the Site Investigation Report, the sites have properties equivalent of a Type 5 soil, which has a runoff rate of 8.66 l/s/ha. However, in line with DCC requirements, the attenuation calculations undertaken, have limited the outflow rate to a maximum of 2.0 l/s/ha, by using a soil type 2 for progression of the calculations. The reason for this limitation, is that the Flood Risk Assessment submitted under a separate cover, has identified a downstream area of the Camac River of being at risk of flooding. The Council, already aware of this issue, confirmed in the preliminary surface water strategy meeting, that our early-stage modelling of the attenuation volume requirements was correct in applying the max outfall rate of 2 l/s/ha to our calculations. An extract of the Control Discharge Limits Table from the Council's SuDS Design & Evaluation guide is shown in *Figure 4* below.

| | 1-in-1 year rainfall (maximum outflow rate)l | 1-in-100 year rainfall (maximum outflow rate) | Long term storage- volume control |
|--|---|--|---|
| Discharge to a combined sewer or location where there is a known downstream capacity issues / flood risk | 2 l/s/ha | 2 l/s/ha | No |
| Discharge to a surface water sewer or watercourse (no known flood risk or capacity issues) Criterion 2.1, 2.2, 4.1, 4.2 | 1-in-1 year greenfield rate | 1-in-100 year greenfield rate | Yes |
| Discharge to a surface water sewer or watercourse (no known flood risk or capacity issues) Criterion 4.3 | Qbar/ Qmed | Qbar/ Qmed | No |

Figure 4 | Permitted Outflow Rates as per SuDS Design & Evaluation Guide Document

For storm water management purposes, it is proposed to divide the sites into four separate sub-catchments, as shown in *Figure 5* below.

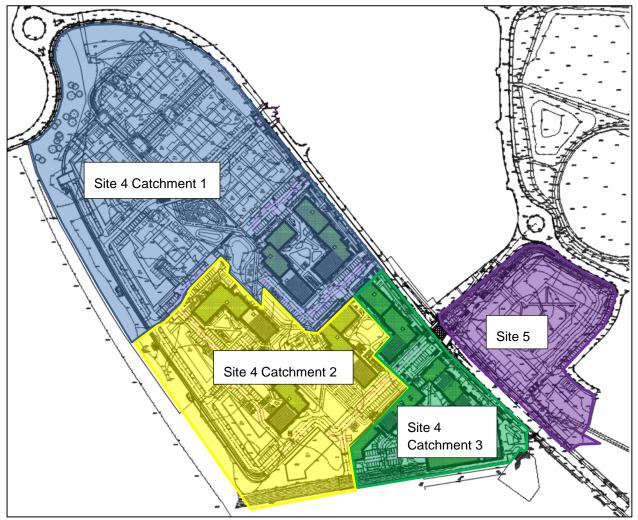


Figure 5 | Sketch of Catchments Template

Storm water from each catchment will be attenuated and discharge at a controlled rate, limited to a maximum of 2 l/s/ha (as per Dublin City Council requirements), to ultimately outfall to the existing surface water networks at Cedar Brook Way and Barnville Walk. The proposed development has been designed to incorporate best drainage practice.

It is proposed to incorporate a Storm Water Management Plan through the use of various SuDS techniques to treat and minimise surface water runoff from the site. The methodology involved in developing a Storm Water Management Plan for the subject site is based on recommendations set out in the Greater Dublin Strategic Drainage Study (GDSDS), Dublin City Council's SuDS Design and Evaluation Guide, and in the CIRIA Report C753 The SuDS Manual. Based on three key elements – Water Quantity, Water Quality and Amenity – the targets of the CIRIA Report C SuDS train concept have been implemented in the design, providing SuDS devices for each of the following:

- Source Control
- Site Control
- o Regional Control

4.2.1 Source Control

Permeable Paving:

It is proposed to introduce permeable paving at all private driveways and parking courts throughout the development. Downpipes from the front of the houses and apartments will drain to filter drains beneath the permeable paving to facilitate maximum infiltration of surface water from driveways and roof areas.

The goal of permeable paving is to control stormwater at the source to reduce runoff. In addition to reducing surface runoff, permeable paving has the dual benefit of improving water quality by trapping suspended solids and filtering pollutants in the substrata layers.

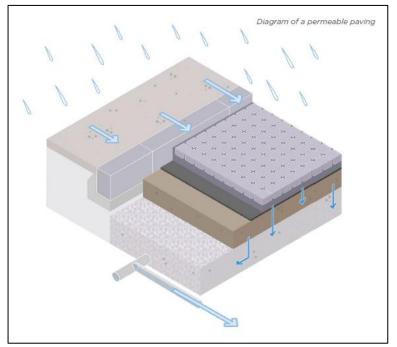


Figure 6 | Illustration of Permeable Paving Extracted from the SuDS Design & Evaluation Guide

Filter Drains:

It is proposed to install filter drains, consisting of perforated pipes surrounded in filter stone around the perimeter of each apartment block. The filter drains will provide infiltration, optimise the retention time, and provide quality improvement to the storm water runoff, in particular to the first flush from hardstanding areas. The proposed perforated pipes connect to the proposed surface water sewer network.

Green / Sedum Roof:

As per the Dublin City Council Green & Blue Roof Guide (2021), it is proposed to introduce a green sedum roofing as a source control device on the roofs of all apartment blocks and commercial buildings on Phases 1, 3, & 4. Phase 2 comprises residential house and duplex type units which are not considered suitable for the incorporation of green or blue roofing measures.

Green roofs have been selected over blue roofs for the following reasons:

• There is ample open space onsite to allow for attenuation at surface level.

- The majority of attenuated surface water will be generated by hardstanding areas at surface level, such as parking bays/courts, roads, and footpaths.
- Utilisation of green roofing ties in well to the overall SuDS strategy and central green corridor and adds increased biodiversity and amenity value.
- The project ecologist has noted that while there is no evidence of bat roosts on-site, evidence of bat foraging has been found. A suitable planting scheme on the green roofs will attract aphid and invertebrate species which will provide a food source for urban birds and bats.
- Green roofs were proposed to be utilised on-site as part of our strategy discussions with Dublin City Council.

Section 3.13 of the Council's Green and Blue Roof Guide notes that where a biodiverse green/blue roof is proposed, a seed mix that replicates Irish grassland habitats of Irish Origin is preferred as far as possible. The project's Landscape Architects have ultimate responsibility for the material design of the planting selection for the proposed green roofs and will design this in consultation with the Project Ecologist in order to produce a suitable landscape for aphids and invertebrate species in order to maintain and encourage these areas as suitable bat foraging location. The Council's guide further advises that if required, consultation requests can be directed to the Authority's Parks, Biodiversity, and Landscape Departments and their officers.

The quantum of green roofing proposed has been coordinated with the M&E designers as photovoltaic (PV) cells will also be required to be installed at roof level on these buildings. The M&E designers have specified that 30% of the roof area is required for the installation of the PV cells. A further 10% has been afforded to allow for the circulation/access routes and roof level plant/fittings. As such it is proposed that 60% of the total quantum of roof area will be dedicated to intensive green roofing. This in accordance with the Dublin City Council Green & Blue Rood Guide 2021, Section 2.0, Green blue roof requirements – area coverage, which specifies a minimum of 50% coverage for intensive green roofs.

| Type of green roof | Minimum coverage (% of total roof area being developed) |
|--------------------|---|
| Extensive | 70% |
| Intensive | 50% |
| | |

Figure 7 | Intensive vs. Extensive Coverage Areas as per the Council's Green and Blue Roof Guide

Intensive green roofs are defined as having a 200mm minimum substrate depth and are suitable for providing planting with habitat complexity, which is suitable for encouraging biodiversity, as per Section 1.2 of the Council's Green and Blue Roof Guide. While it is also noted in this section that intensive roofs are typically planted with grass and sedum, it is proposed that the planting regime to be designed and employed by the Landscape Architects will maintain, and encourage these areas, as suitable for continued bird and bat foraging locations.

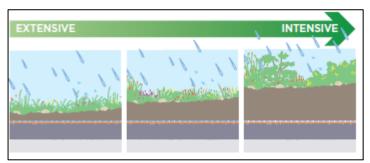


Figure 8 | Illustrative Cross Section of Green Roof Types as per the Council's Green and Blue Roof Guide

In summary, it is proposed to cover 60% of the total suitable roof space with an intensive green roof with a substrate depth of 200mm minimum, totalling a cumulative green roof area of 14,909m². This measurement is based upon the full masterplan layout. The indicative roof plan for the green roofs and PV cells is shown on Drawing Number: 22-010-P240.

The substrate and the plant layers in a green roof absorb large amounts of rainwater and release it back into the atmosphere by transpiration and evaporation. They also filter water as it passes through the layers, so the run-off, when it is produced, has fewer pollutants. Rainfall not retained by green roofs is detained, effectively increasing the time to peak, and slowing peak flows.

4.2.2 Site Control

Roadside Bio-retention Tree Pits:

It is proposed to provide roadside trees throughout the development. Trees can help control storm water runoff because their leaves, stems, and roots slow rain from reaching the ground and capture and store rainfall to be released later. Trees help to attenuate flows, trap silts and pollutants, promote infiltration, and prevent erosion. Incorporating tree planting offers multiple benefits, including attractive planting features, improved air quality and increased biodiversity whilst helping to ensure adaptation to climate change.

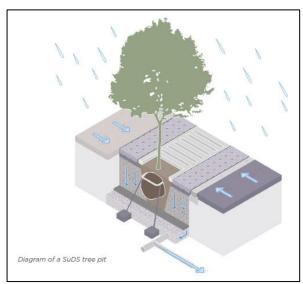


Figure 9 | Illustration of a Tree Pit Extracted from the SuDS Design & Evaluation Guide

Swales:

Swales are grassed channels proposed to run parallel and adjacent to selected roads throughout the site. Rainfall from the road surface will be directed to gaps in the road kerbing and will flow to the swales. The swales will be linked back to the drainage network to prevent flooding in extreme weather events, where the volume of rainfall exceeds the percolation capacity of the swales. An extract from Drawing Number: 22-010-P240 shows an illustration of the gapped kerbing construction.

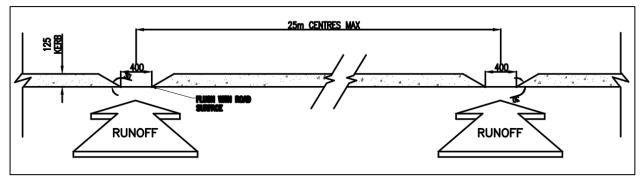


Figure 10 | Gapped Kerbing Extract from Drawing Number: 22-010-P240

There is intended to be several pedestrian crossings over the long swale adjacent Road 1. These crossings will not interrupt the swale, which will incorporate short piped connections as per *Figure 11* overleaf, which has been extracted from Section 8.4.5 of the SuDS Design & Evaluation Guide. Check dams are small, gapped, walls which lie across the width of swales at regular intervals, and are proposed to be incorporated to the swales. These check dams allow the surface water flowing through a swale to have a reduced velocity, increasing its retention time in the swale, and the surface water absorption volume to the soil.



Figure 11 | Examples of Swale Crossings and Check Dams

Grassed swales enhance surface water runoff quality as they slow down water flow, allowing suspended particles to filter and settle out of suspension.

362 linear metres of swales are proposed as part of the development.

Bio-retention Systems (Raingardens):

Bio-retention planted areas will be provided within the private domain around apartment blocks. Planted boxes will intercept down pipes from the apartment blocks.

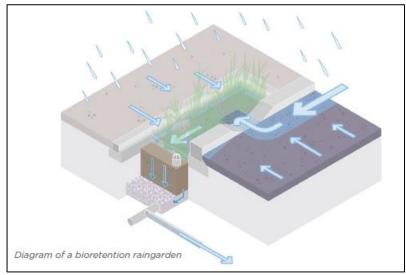


Figure 12 | Illustration of a Raingarden Extract from the SuDS Design & Evaluation Guide

4.2.3 Regional Control

Detention Basin

Detention basins are proposed to be utilised for attenuation of surface water. These basins can be utilised during regular weather conditions for other purposes and will only fill with water during heavier rainfall events. Detention basins are engineered depressions in the ground and are typically seeded with grass and may also be suitable for planting. Detention basins may be further utilised as recreational/play areas, an option which has been utilised in the proposals for this project. A prime example of this incorporated to the project is Basin 4, which performs the role of a "*multi-functional SuDS component*" which will act as a sports court during dry weather and an attenuation area during heavier rainfall events, as per the figure included on Page 15 of the Council's SuDS Design & Evaluation guide. The entry invert levels of the pipes to the multipurpose area have been designed in such a way that it will be the last of the attenuation areas to fill and water will only be retained here during the heaviest of rainfall events, ensuring that it can be utilised in its role as a play facility more often. An extract from Drawing Number: 22-010-P240 is included as *Figure 13* showing this multi-purpose court and basin, below.



Figure 13 | Extract from 22-010-P240

Attenuation tanks:

Underground attenuation tanks are also proposed to be utilised for the attenuation of surface water. These will attenuate water volumes underground. Each attenuation tank/system has been sized in conjunction with the basin attenuation volumes to accommodate attenuation from catchments for rainfall events greater than the 1-in-100-year event.

The basement level attenuation tank will remain under private management.

Flow Control:

A flow control device (Hydrobrake or similar approved) is proposed at each sub-catchment attenuation feature, which will limit exiting flows to a maximum rate of 2l/s/ha as permitted by DCC.

Petrol interceptor:

Class 1 petrol interceptors will be provided before the surface water outfalls to the local surface water networks.

Rainwater butts are not considered suitable due to the scale of the development (large residential and commercial blocks). The site investigation report results indicate that the subsoil infiltration rates are not conducive to successful integration of soakaways to the design.

4.3 SuDS Maintenance Regime

A maintenance regime for the SuDS features will be incorporated to the Operation and Maintenance manual for the development. Surface SuDS features can typically be maintained as part of the regular maintenance of the landscape, incorporating litter picking, grass cutting, and inspections. *Figure 14* overleaf, is an extract from Section 12.3 of the SuDS Design & Evaluation Guide, and generally describes the regular maintenance aspect for the SuDS.

| Туре | Activity | Normal site care (Site) or SuDS-specific maintenance | Suggested frequency |
|---------------------|--|---|--|
| Regular M | aintenance | (SuDS) | |
| Litter | Pick up all litter in SUDS Landscape areas along with remainder of the site – remove from site | Site | 1 visit monthly |
| Grass | Mow all grass verges, paths and amenity grass at 35-50mm with 75mm max. Leaving cuttings in situ | Site | As required or 1 visit monthly |
| Grass | Mow all dry swales, dry SUDS basins and margins to low flow channels and other SUDS features at 100mm with 150mm max. Cut wet swales or basins annually as wildflower areas – 1st and last cuts to be collected | Site | 4-8 visits per year or as required |
| Grass | Wildflower areas strimmed to 100mm in Sept or at end of school holidays – all cuttings removed Or Wildflower areas strimmed to 100mm on 3 year rotation – 30% each year – all cuttings removed | Site | 1 visit annually 1 visit annually |
| Inlets & outlets | Inspect monthly, remove silt from slab aprons and debris. Strim 1m round for access | SuDS | 1 visit monthly |
| Permeable paving | Sweep all paving regularly to keep surface tidy | Site | 1 visit annually or as required |

Figure 14 | Regular Maintenance Requirements for SuDS

There will still be a remaining requirement for more intensive maintenance tasks to be undertaken however, the severity of these tasks can be reduced by regular inspections and proactive responses being incorporated as a part of the regular maintenance regime discussed above. A table showing the typical requirements for the occasional maintenance tasks and remedial works is extracted from the SuDS Design & Evaluation Guide to the figure overleaf.

| Permeable paving | Sweep and suction brush permeable paving when ponding occurs | SuDS | As required - | | |
|---------------------|--|-------------|----------------------------------|--|--|
| | | | estimate 10-15 year intervals | | |
| Flow controls | Annual inspection of control chambers - remove silt and check free flow | | | | |
| Wetland & pond | Wetland vegetation to be cut at 100mm on 3 – 5 year rotation or 30% each year. All cuttings to be removed to wildlife piles or from site. | Site | As required | | |
| Silt | Inspect swales, ponds, wetlands annually for silt accumulation | Site & SuDS | 1 visit annually | | |
| Silt | Excavate silt, stack and dry within 10m of Site & SuDS As returned by Subscription Site & SuDS As returned by Subscription Site & Subscription Sit | | | | |
| Native planting | Remove lower branches where necessary to ensure good ground cover to protect soil profile from erosion. | SuDS | 1 visit annually | | |
| Remedial Work | | | | | |
| General SuDS | Inspect SuDS system to check for damage or failure when carrying out other tasks. Undertake remedial work as required. | SuDS | Monthly As required | | |

Figure 15 | Further Maintenance Requirements for SuDS

4.4 Interception of Treatment Storage and Attenuation Storage

As noted above, the methodology involved in developing the Storm Water Management Plan for the subject site is based on recommendations set out in the Greater Dublin Strategic Drainage Study (GDSDS). DCC's SuDS Design and Evaluation Guide 2021, and in the CIRIA Report C753 The SuDS Manual. Appendix E of the Greater Dublin Strategic Drainage Study (GDSDS) sets out criteria for determining the provision of interception or treatment storage, attenuation storage and long-term storage at a development site. These calculations are summarised below. Please note that for the following calculations:

- The calculations have been progressed for the full masterplan development comprising Sites 4 & 5, unless specified otherwise.
- The site area measurement is deemed to be the blueline boundary (ownership boundary as per *Figure 1*) and excludes the public domain area. The reason for this exclusion is that the existing roads and footpaths are already served by the existing road gullies and surface water network infrastructure.

While Section 3.5 of the Council's Green and Blue Roof Guide advises that green roofs provide an
element of short-term storage and reduced runoff via evapotranspiration, for the purpose of
producing the volumetric attenuation requirement calculations, green roofs for this project have
been considered as paved surfaces (hardstanding areas) for the progression of these calculations.

4.4.1 Criterion 1: River Water Quality Protection

Water Quality Standard 1: Interception

The Greater Dublin Strategic Drainage Study (GDSDS) states that approximately 30% to 40% of rainfall events are sufficiently small that there is no measurable runoff from greenfield areas into the receiving waters. These events are generally considered as the first 5mm of rainfall. Assuming 80% runoff from paved surfaces and 0% from pervious surfaces for the first 5mm of rainfall yields the following:

| | 138,311m ² x 0.62 x 0.75 = | 138,311m² site area | |
|--|---------------------------------------|-----------------------------|--|
| Paved surfaces connected to drainage system | 64 04 Em2 | 62% of the site is paved | |
| diamage system | 64,315m ² | 75% of the paved area | |
| | 64,315m ² x 5mm x 0.8 = | Paved area directly drained | |
| Volume of Interception Storage | 057.003 | 5mm rainfall depth | |
| | 257.26m ³ | 80% paved runoff factor | |

Table 4 | Interception Calculation

This is further in line with Section 4.2.2 of the CIRIA Report C753 The SuDS Manual, which identifies Water Quality Criterion 1 as required to "*Support the management of water quality in receiving waters and groundwaters*". The section further lists methods whereby this can be achieved: Pollution Prevention, Interception, Treatment, & Maintenance and remedial work. Section 4.3.1 of the same document discusses the requirements for provided sufficient interception methods via the introduction of Green Roofs, Pervious Surfaces, & Vegetated SuDS.

It has been calculated that the interception volume as noted above will be provided through the introduction of nature-based SuDS to the design as follows:

Permeable paving is proposed in private driveways and parking courts and accounts for a total cumulative area of C. 6,684m². Assuming a subbase depth of 0.4m with 33% voids, this yields a treatment volume of 882m³. The permeable paving locations can be seen on drawing number 22-010-P010 Surfacing Layout. These figures are based on the masterplan layout for Site 4 but does not include any permeable paving which may be later proposed as part of the detailed design of Site 5, which will be the subject of a later planning application.

As noted above, the green roofing amounts to a cumulative area of approximately 14,909m² and shall consist of 200mm substrate minimum. Assuming a 30% water volume retention, this amounts to approximately 894m³ of treatment storage volume.

Filter drains, swales, raingardens, and roadside trees around the site provide further treatment volume.

These SuDS features provide ample treatment volume to meet the volumetric interception requirements.

SuDS features are identified on the SuDS Layout Drawing, refer to 22-010-P240, submitted as part of the planning package.

4.4.2 Criterion 2: River Regime Protection

Attenuation storage is provided to limit the discharge rate from the site into receiving waters. As per the GDSDS, the required attenuation volume is calculated assuming 80% runoff from paved areas (20% assumed as permeable paved parking bays, excludes calculations for apartment blocks which have been calculated as 100%), and has been calculated for the 1-year, 30-year and 100-year return periods, identifying the critical storm for each – refer to calculations included in Appendix A.

The calculations included in Appendix A have been based on the usage of an outflow rate of 1.991 l/s/ha, in line with DCC's requirement for a max permitted value of 2 l/s/ha.

As noted above, Site 4 has been divided in to 3 sub-catchments, with Site 5 its own catchment. However, 2 of the sub-catchments for Site 4, catchments 1 & 2, will run in a chain-like system to outfall to the public SW water network. This means that Catchment 1 will flow through Catchment 2 before outfalling to the public surface water network. Subsequently, the hydrobrake limit for Catchment 2 will be the sum of the permitted outflow rate for Catchments 1 & 2.

Based on the calculations, included as Appendix A, the required attenuation storage volume for each subcatchment is set out in *Table 5* below, as well as the permitted outflow rate per catchment, and the actual outflow rate of the catchments running in the chain system.

| Catchment | Area | Allowable Discharge Rate (Per Catchment) | Allowable Discharge Rate (accounting for Chain System) | Required Attenuation Volume |
|-----------------------------|---------|--|--|-----------------------------------|
| | m² | l/s | l/s | m ³ |
| Catchment 1: Site 4 North | 60,290 | 11.82 | 11.82 | 1,800 |
| Catchment 2: Site 4 Central | 33,711 | 7.54 | 19.36 | 800 |
| Catchment 3: Site 4 South | 16,868 | 3.36 | 3.36 | 1,100 |
| Catchment 4: Site 5 | 18,166 | 3.20 | 3.20 | 1,00 |
| Total | 129,035 | 25.92 | - | 4,700 |

Table 5 | Attenuation Volume for Each Sub-Catchment

It should be noted that the figures provided in the table above, and the calculations in Appendix A for Site 5 are indicative only, for the purpose of this masterplan submission and that Site 5 will be subject to a future detailed planning permission application.

In order to cater for the full attenuation requirement, detention basins and tanks have been incorporated to the design. There is an attenuation tank located in the basement of the southern blocks complex, with detention basins and further attenuation tanks located in the central green corridor. The attenuation areas have been designed to ensure the required attenuation volume is catered for and that there will be no surcharging of the tanks or basins for up to the 1-in-100 year storm incorporating an additional 20% for climate change. The attenuation volumes provided in the detention basins and tanks are recorded to *Table 6*, overleaf.

| Location | Attenuation volume provided | |
|-------------|--------------------------------|--|
| | <i>m</i> ³ | |
| Catchment 1 | 1,918 | |
| Catchment 2 | 813 | |
| Catchment 3 | 1,122 | |
| Catchment 4 | 1,000 | |
| Total | 4,853 | |

Table 6 | Attenuation Volume Provision

As per *Table 5 & 6*, the required attenuation volume is 4,700m³, with 4,853m³ of attenuation volume actually provided.

Please note that given the masterplan development in mainly comprised of apartment, duplex, and commercial blocks with their associated private green spaces to be controlled by a management company, there is limited to no scope for urban creep, and as such these have not been factors to the attenuation calculations previously discussed.

The finished floor levels of surrounding building have been designed to be at least 0.5m above the Top of Water levels of the nearby detention basins as applicable. The Top of Water levels for the basins for the 1 in 100-year storm event have been calculated to be:

Catchment 1: 55.65mOD

Catchment 2: 56.25mOD

Catchment 3: 55.65mOD

4.4.3 Criterion 3: Levels of Service

There are four criteria for levels of service. These are:

- <u>Criterion 3.1:</u> No external flooding except where specifically planned (30-year high intensity rainfall event).
- <u>Criterion 3.2:</u> No internal flooding (100-year high intensity rainfall event).
- <u>Criterion 3.3:</u> No internal flooding (100-year river event and critical duration for site storage).
- <u>Criterion 3.4:</u> No flood routing off site except where specifically planned (100-year high intensity rainfall event).

Both internal and external flooding have been assessed in the Flood Risk Assessment report which accompanies this Engineering Assessment Report. The Flood Risk Assessment has been carried out in

accordance with the *DEHLG/OPW Guidelines on the Planning Process and Flood Risk Management* published in November 2009.

This report has identified that the site lies within Flood Zone C and is separated from sites identified as being in Flood zone A & B both topographically and with sufficient separation distance. The subject site is a suitable location for the proposed development. Thusly, justification tests are not required to be undertaken. There are currently no floodplains identified on-site nor are any proposed as part of the subject development design. Further Flood Risk Assessment details are extracted to Section 4.6 of this report.

The assessment identifies the risk of both internal and external flooding at the site from various sources and sets out mitigation measures against the potential risks of flooding. The sources of possible flooding assessed in the report include coastal, fluvial, pluvial (direct heavy rain), groundwater and human/mechanical errors.

As a result of the flood risk management and mitigation measures proposed, the residual risk of internal or external flooding for the 30-year and 100-year flood events is low, and accordingly all four of the above criteria have been met. Please refer to the accompanying Flood Risk Assessment report for the full analysis of the flood risk at the subject site.

4.4.4 Criterion 4: River Flood Protection

The long-term storage volume is a comparison of pre- and post-development runoff volumes. The objective is to limit the runoff discharged after development to the same as that which occurred prior to development.

Of the three methods described in the GDSDS for establishing River Flood Protection by comparison of the pre- and post-development runoff volumes, (Criteria 4.1, 4.2 and 4.3 respectively), Criteria 4.3 is selected for use as the most practical criteria at this stage in the design.

The Criteria 4.3 approach is for all runoff to be limited to either Q_{BAR} or to 2 l/s/Ha, whichever is the greater. However, DCC policy instructs that a max outflow rate of 2 l/s/ha is permitted. The proposed drainage system includes flow control devices at the outfall for each catchment to ensure that the discharge rate is limited to the permitted outflow rate, and ample attenuation is provided for the 1-in-100 year storm, accounting for a 20% increase due to climate change.

The extra runoff volume of the development runoff over greenfield runoff, Vol_{xs} , has been calculated for each of the sub-catchments. Note that as stated in the GDSDS, this volume is not additional to the attenuation storage volume but is effectively an element of it.

4.5 Surface Water - General

The proposed drainage and attenuation strategy drawings are included as part of the planning package and can be seen on drawing numbers:

- 22-010 -P200-P203 and P205.
- Surface water catchments on 22-010-P210.
- The SuDS layout drawing is 22-010-P240.
- A cross section of the central attenuation corridor is provided on 22-010-P250.
- Ancillary details drawings for the Typical Surface Water Details are on 22-010-P230.

• The Typical SuDS Details are provided on 22-010-P241.

Surface water long sections have been prepared in line with the Development Plan requirements for the preparation of a Surface Water Management Plan Report and are submitted as Drawing Numbers: 22-010-P250, & 22-010-P260 & P261.

Surface water sewers will generally consist of PVC (to IS 123) or concrete socket and spigot pipes (to IS 6) and laid strictly in accordance with Dublin City Council requirements for taking in charge. It is intended that all sewers within the public domain will be handed over to Dublin City Council for taking in charge.

All private outfall manholes will be built in accordance with the Greater Dublin Regional Code of Practice for Drainage Works. No private drainage will be located within public areas.

Drains will be laid in accordance with the requirements of the Building Regulations, Technical Guidance Document H.

All SuDS and surface water drainage networks proposed in the public domain will be constructed to the standards required for Taking in Charge.

As is standard, the proposed Surface Water network, including SuDS devices will be constructed in accordance with the requirements of the various utility provides such as in respect to separation distance between utilities etc.

Typically, there are no existing utilities internal to the site (gas/telecommunications etc)., with the exception of overhead electricity lines. It is intended that these overhead lines will be undergrounded as part of the site work, however, ESB will not engage on this matter until a grant of planning permission has been received. The proposal/design for the undergrounding of overhead lines will be undertaken at the appropriate time.

4.6 Flood Risk Assessment

As previously noted, a site-specific Flood Risk Assessment has been carried out for the proposed development and accompanies this submission under separate cover.

This report identifies that the site is located in an area designated as Flood Zone C, which is suitable for the proposed development.

There have been no flood plains identified on site, nor are any proposed as part of the subject development design.

Overland flood routing has been incorporated to the design. Should fluvial flooding occur, surface water can flow overland towards the attenuation areas and ditch networks via open spaces as shown in the figure overleaf. This figure is extracted from Drawing Number: 22-010-P220 which is submitted as part of the planning package.

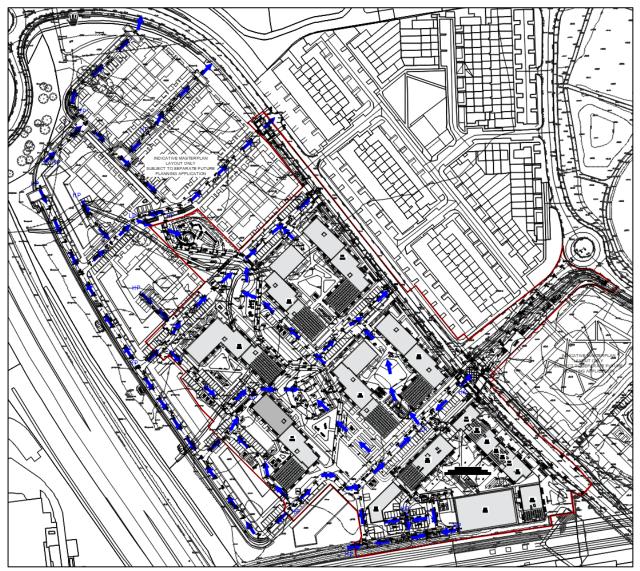


Figure 16 | Overland Flood Route

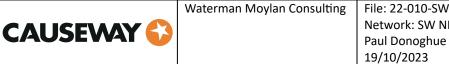
The Flood Risk Assessment discusses in detail the various sources, pathways, receptors, likelihood, consequence, and risk of flooding. The identified risks are mitigated and the residual risk assessed. A summary is provided in *Table 7*, overleaf.

| Source | Pathway | Receptor | Likelihood | Consequence | Risk | Mitigation Measure | Residual Risk |
|-------------------------------|--|---|-------------------------------|-------------|----------------------------|---|------------------|
| Tidal | Irish Sea (River Liffey) | Proposed development | Extremely low | None | Negligible | None | Negligible |
| Fluvial | Blackditch Stream & River Camac | Proposed development | Low | Low | Extremely Low | Setting of floor levels, overland flood routing | Extremely Low |
| Pluvial | Private & Public Drainage Network | Proposed development, downstream properties, and roads | Ranges from high to low | Moderate | Ranges from high to low | Appropriate drainage, SuDS, and attenuation design, setting of floor levels, overland flood routing | Low |
| Ground Water | Ground | Underground services, ground and undercroft level of buildings, roads | High | Moderate | High | Appropriate setting of floor levels, flood routing, damp proof membranes | Low |
| Human/ Mechanical Error | Drainage network | Proposed development | High | Moderate | High | Setting of floor levels, overland flood routing, regular inspection of SW network | Low |

Table 7 | Summary of the Flood Risks from the Various Components

Appendices

A. GDSDS Attenuation Calculations



Design Settings

| Rainfall Methodology | FSR | Maximum Time of Concentration (mins) | 30.00 |
|-----------------------|----------------------|--------------------------------------|---------------|
| Return Period (years) | 5 | Maximum Rainfall (mm/hr) | 50.0 |
| Additional Flow (%) | 0 | Minimum Velocity (m/s) | 1.00 |
| FSR Region | Scotland and Ireland | Connection Type | Level Soffits |
| M5-60 (mm) | 16.800 | Minimum Backdrop Height (m) | 0.200 |
| Ratio-R | 0.300 | Preferred Cover Depth (m) | 1.200 |
| CV | 1.000 | Include Intermediate Ground | \checkmark |
| Time of Entry (mins) | 4.00 | Enforce best practice design rules | х |

<u>Nodes</u>

| Name | Area (ha) | T of E (mins) | Cover Level (m) | Diameter (mm) | Easting (m) | Northing (m) | Depth (m) |
|----------|----------------|------------------|-----------------------|------------------|--------------------------|--------------------------|----------------|
| 1 | 0.090 | 4.00 | 57.320 | 1200 | 707582.615 | 733130.913 | 1.120 |
| 2 | 0.094 | 4.00 | 57.300 | 1200 | 707631.554 | 733179.070 | 1.558 |
| 3 | 0.118 | 4.00 | 57.160 | 1200 | 707646.088 | 733103.044 | 1.230 |
| 4 | 0.143 | 4.00 | 56.800 | 1200 | 707686.346 | 733143.264 | 1.535 |
| 5 | 0.186 | 4.00 | 56.680 | 1200 | 707678.677 | 733040.140 | 1.240 |
| 6 | 0.186 | 4.00 | 56.180 | 1200 | 707731.036 | 733092.449 | 1.253 |
| 7 | 0.060 | 4.00 | 56.000 | 1350 | 707766.868 | 733047.149 | 1.575 |
| 8 | 0.058 | 4.00 | 55.830 | 1200 | 707795.011 | 733011.704 | 1.125 |
| 9 | 0.058 | 4.00 | 56.050 | 1200 | 707776.870 | 733035.010 | 1.493 |
| 10 | 0.060 | 4.00 | 55.830 | 1200 | 707767.760 | 733033.825 | 1.530 |
| 11 | 0.060 | 4.00 | 56.020 | 1200 | 707753.222 | 733019.219 | 1.864 |
| 12 | 0.057 | 4.00 | 56.080 | 1200 | 707748.849 | 733007.619 | 1.790 |
| 13 | 0.098 | 4.00 | 56.170 | 1200 | 707739.264 | 733008.337 | 2.100 |
| 14 | 0.824 | 4.00 | 57.220 | 1200 | 707552.358 | 733030.718 | 1.450 |
| 15 | 0.082 | 4.00 | 56.810 | 1200 | 707580.419 | 732974.310 | 1.535 |
| 16 | | | 56.900 | 1200 | 707583.499 | 732975.911 | 1.814 |
| 17 | 0.020 | 4.00 | 56.900 | 1200 | 707588.629 | 733018.388 | 1.500 |
| 18 | 0.085 | 4.00 | 56.750 | 1200 | 707607.207 | 732999.605 | 1.832 |
| 19 | 0.848 | 4.00 | 56.550 | 1200 | 707623.498 | 733015.910 | 1.799 |
| 20 | 0.022 | 4.00 | 57.600 | 1200 | 707557.536 | 733073.568 | 1.425 |
| 21 | 0.080 | 4.00 | 57.450 | 1200 | 707582.693 | 733098.703 | 1.986 |
| 22 | 0.118 | 4.00 | 57.240 | 1200 | 707639.436 | 733091.309 | 1.425 |
| 23 | 0.212 | 4.00 | 57.140 | 1200 | 707614.894 | 733066.788 | 2.279 |
| 24 | 0.215 | 4.00 | 56.860 | 1200 | 707655.360 | 733026.683 | 2.670 |
| 25 | | | 57.000 | 1200 | 707667.633 | 733023.067 | 2.853 |
| 26 | | | 55.150 | 1200 | 707672.207 | 732986.631 | 1.117 |
| 27 | | | 55.150 | 1200 | 707691.305 | 732984.076 | 1.181 |
| 28 | 0.057 | 4.00 | 57.000 | 1200 | 707712.245 | 732992.966 | 1.925 |
| 29 | 0.057 | 4.00 | 55.150 | 1200 | 707708.670 | 732977.575 | 1.243 |
| 30 | 0.083 | 4.00 | 56.830 | 1200 | 707590.871 | 732955.923 | 0.930 |
| 31 | 0.832 | 4.00 | 57.450 | 1200 | 707627.313 | 732896.089 | 2.242 |
| 32 | 0.040 | 4.00 | 57.600 | 1200 | 707635.462 | 732901.380 | 2.441 |
| 33 | 0.040 | 4.00 | 57.050 | 1200 | 707651.237 | 732917.100 | 2.336 |
| 34 | 0.028 | 4.00 | 57.020 | 1200 | 707638.572 | 732948.769 | 1.370 |
| 35 | 0.028 | 4.00 | 56.830 | 1200 | 707654.753 | 732932.519 | 1.295 |
| 36 37 | 0.090 | 4.00 4.00 | 56.860 | 1200 1200 | 707662.206 707647.642 | 732933.154 | 2.431 1.491 |
| 37 | 0.054 0.061 | 4.00 | 56.700 | 1200 | 707689.219 | 733001.609 732960.032 | 2.108 |
| 38 | 0.001 | 4.00 | 56.410 55.150 | 1200 | 707689.219 | 732950.032 | 1.335 |
| 40 | 0.058 | 4.00 | 55.750 | 1200 | 707809.094 | 732993.635 | 0.925 |
| 40 | 0.058 | 4.00 | 55.750 | 1200 | 707830.504 | 732966.107 | 1.425 |
| 41 | 0.050 | 4.00 | JJ./JU | 1200 | 707030.304 | / 32300.10/ | 1.423 |

<u>Nodes</u>

| Name | Area (ha) | T of E (mins) | Cover Level (m) | Diameter (mm) | Easting (m) | Northing (m) | Depth (m) |
|----------|----------------|------------------|-----------------------|------------------|--------------------------|--------------------------|----------------|
| 42 | 0.029 | 4.00 | 56.050 | 1200 | 707830.561 | 732959.010 | 1.760 |
| 43 | 0.029 | 4.00 | 56.060 | 1200 | 707808.187 | 732936.671 | 1.928 |
| 44 | 0.046 | 4.00 | 56.240 | 1200 | 707793.010 | 732925.360 | 2.278 |
| 45 | 0.056 | 4.00 | 56.630 | 1200 | 707773.973 | 732906.324 | 2.776 |
| 46 | 0.058 | 4.00 | 56.400 | 1200 | 707731.229 | 732948.695 | 2.787 |
| 47 | 0.058 | 4.00 | 56.300 | 1200 | 707726.510 | 732973.051 | 1.425 |
| 48 | | | 56.450 | 1200 | 707725.039 | 732949.075 | 2.862 |
| 49 | | | 56.570 | 1500 | 707719.676 | 732942.481 | 2.808 |
| 50 | 0.078 | 4.00 | 56.790 | 1200 | 707667.288 | 732838.488 | 1.425 |
| 51 | 0.078 | 4.00 | 57.200 | 1200 | 707633.852 | 732886.667 | 2.128 |
| 52 | 0.055 | 4.00 | 56.690 | 1200 | 707690.123 | 732872.909 | 1.540 |
| 53 | 0.048 | 4.00 | 57.030 | 1200 | 707655.169 | 732907.984 732950.364 | 2.234 |
| 54 55 | 0.085 0.085 | 4.00 4.00 | 56.600 56.700 | 1200 1200 | 707697.549 707747.278 | 732950.364 | 2.004 1.425 |
| 56 | 0.085 | 4.00 | 56.700 | 1200 | 707715.184 | 732932.724 | 2.262 |
| 57 | 0.085 | 4.00 | 56.720 | 1200 | 707722.058 | 732940.127 | 2.202 |
| 58 | | | 55.740 | 1200 | 707731.855 | 732931.029 | 2.025 |
| 59 | | | 55.750 | 1200 | 707758.967 | 732903.921 | 1.065 |
| 60 | | | 56.900 | 1350 | 707765.933 | 732896.955 | 2.300 |
| 61 | 0.058 | 4.00 | 57.410 | 1200 | 707734.942 | 732764.697 | 1.425 |
| 62 | 0.093 | 4.00 | 57.400 | 1200 | 707770.349 | 732800.111 | 1.230 |
| 63 | 0.093 | 4.00 | 57.610 | 1200 | 707754.555 | 732784.314 | 1.839 |
| 64 | 0.043 | 4.00 | 57.170 | 1200 | 707733.946 | 732804.922 | 1.863 |
| 65 | 0.043 | 4.00 | 57.180 | 1200 | 707731.572 | 732816.684 | 1.933 |
| 66 | 0.078 | 4.00 | 57.110 | 1200 | 707713.370 | 732772.930 | 1.400 |
| 67 | 0.078 | 4.00 | 56.800 | 1200 | 707679.556 | 732820.801 | 1.556 |
| 68 | 0.081 | 4.00 | 56.750 | 1200 | 707703.518 | 732844.753 | 1.776 |
| 69 | 0.043 | 4.00 | 56.800 | 1200 | 707715.962 | 732866.502 | 1.951 |
| 70 | 0.085 | 4.00 | 56.800 | 1200 | 707729.757 | 732880.144 | 2.091 |
| 71 | 0.043 | 4.00 | 57.100 | 1200 | 707785.360 | 732827.871 | 1.425 |
| 72 | 0.043 | 4.00 | 57.100 | 1200 | 707775.426 | 732843.654 | 1.611 |
| 73 | 0.043 | 4.00 | 56.700 56.700 | 1200 | 707740.545 | 732878.534 | 2.027 |
| 74 75 | 0.119 | 4.00 | 56.520 | 1350 1200 | 707749.441 707859.264 | 732887.430 732852.421 | 2.069 1.430 |
| 76 | 0.046 | 4.00 | 57.020 | 1200 | 707804.877 | 732798.070 | 1.430 |
| 77 | 0.040 | 4.00 | 57.620 | 1350 | 707829.427 | 732822.604 | 2.750 |
| 78 | 0.005 | | 57.000 | 1350 | 707791.921 | 732860.029 | 2.370 |
| 79 | 0.030 | 4.00 | 56.000 | 1350 | 707779.375 | 732862.434 | 1.413 |
| 80 | 0.030 | 4.00 | 56.000 | 1350 | 707766.010 | 732884.373 | 1.574 |
| 81 | 0.073 | 4.00 | 57.000 | 1200 | 707824.072 | 732839.343 | 1.125 |
| 82 | 0.078 | 4.00 | 57.000 | 1200 | 707793.051 | 732870.402 | 2.003 |
| 83 | 0.078 | 4.00 | 56.860 | 1350 | 707777.022 | 732896.708 | 2.595 |
| 84 | | | 56.580 | 1800 | 707777.981 | 732907.503 | 2.370 |
| 85 | | | 56.240 | 1200 | 707797.658 | 732927.180 | 2.130 |
| 86 | | | 56.020 | 1200 | 707807.268 | 732934.340 | 1.950 |
| 87 | | | 56.900 | 1200 | 707834.498 | 732961.081 | 2.957 |
| 88 | 0.025 | 4.00 | 55.630 | 1200 | 707841.014 | 732964.358 | 1.711 |
| 89 | 0.025 | 4.00 | 57.380 | 1200 | 707813.378 | 732773.344 | 1.425 |
| 90 91 | 0.025 0.029 | 4.00 4.00 | 57.900 58.850 | 1200 1200 | 707816.530 707874.700 | 732753.705 732763.043 | 2.044 1.425 |
| 91 | 0.029 | 4.00 | 58.240 | 1200 | 707849.689 | 732759.028 | 2.552 |
| 93 | 0.128 | 4.00 | 57.840 | 1200 | 707845.749 | 732783.568 | 2.330 |
| | 0.120 | | 2.1040 | 1200 | , e, e e e e e e | | 2.000 |



Page 3

<u>Nodes</u>

| Name | Area (ha) | T of E (mins) | Cover Level (m) | Diameter (mm) | Easting (m) | Northing (m) | Depth (m) |
|---------|--------------|------------------|-----------------------|------------------|----------------|-----------------|--------------|
| 94 | | 4.00 | 56.000 | 1200 | 707885.570 | 732824.307 | 0.430 |
| 95 | 0.133 | 4.00 | 56.000 | 1200 | 707873.258 | 732811.989 | 1.530 |
| 96 | 0.053 | 4.00 | 56.000 | 1200 | 707892.179 | 732793.068 | 1.619 |
| 97 | 0.156 | 4.00 | 56.000 | 1200 | 707922.702 | 732797.973 | 1.722 |
| 98 | 0.118 | 4.00 | 56.000 | 1200 | 707925.756 | 732801.027 | 1.736 |
| 99 | | | 56.000 | 1200 | 707890.793 | 732835.990 | 1.901 |
| 100 | 0.138 | 4.00 | 56.590 | 1200 | 707868.297 | 732858.585 | 2.597 |
| 101 | 0.188 | 4.00 | 59.200 | 1200 | 707962.141 | 732812.736 | 1.425 |
| 102 | 0.237 | 4.00 | 56.820 | 1200 | 707892.325 | 732882.596 | 3.015 |
| 103 | 0.083 | 4.00 | 56.000 | 1200 | 707845.472 | 732946.315 | 1.125 |
| 104 | 0.083 | 4.00 | 56.550 | 1200 | 707881.315 | 732901.600 | 2.057 |
| 105 | | | 56.000 | 1500 | 707896.317 | 732886.586 | 2.214 |
| 106 | | | 56.740 | 1200 | 707899.695 | 732889.962 | 2.970 |
| 107 | | | 56.600 | 1200 | 707892.284 | 732899.924 | 2.955 |
| 107_OUT | | | 56.000 | 1200 | 707907.707 | 732912.208 | 2.421 |

<u>Links</u>

| Name | US Node | DS Node | Length (m) | ks (mm) / n | US IL (m) | DS IL (m) | Fall (m) | Slope (1:X) | Dia (mm) | T of C (mins) | Rain (mm/hr) |
|-------|------------|------------|---------------|----------------|--------------|--------------|-------------|----------------|-------------|------------------|-----------------|
| 1.000 | 1 | 2 | 68.660 | 0.600 | 56.200 | 55.742 | 0.458 | 150.0 | 225 | 5.07 | 50.0 |
| 1.001 | 2 | 4 | 65.454 | 0.600 | 55.742 | 55.415 | 0.327 | 200.0 | 225 | 6.26 | 50.0 |
| 2.000 | 3 | 4 | 56.907 | 0.600 | 55.930 | 55.551 | 0.379 | 150.0 | 225 | 4.89 | 50.0 |
| 1.002 | 4 | 6 | 67.671 | 0.600 | 55.265 | 54.927 | 0.338 | 200.0 | 375 | 7.14 | 50.0 |
| 3.000 | 5 | 6 | 74.011 | 0.600 | 55.440 | 55.070 | 0.370 | 200.0 | 225 | 5.34 | 50.0 |
| 1.003 | 6 | 7 | 57.761 | 0.600 | 54.927 | 54.514 | 0.413 | 140.0 | 375 | 7.77 | 50.0 |
| 1.004 | 7 | 10 | 13.354 | 0.600 | 54.425 | 54.358 | 0.067 | 200.0 | 450 | 7.93 | 50.0 |
| 4.000 | 8 | 9 | 29.534 | 0.600 | 54.705 | 54.557 | 0.148 | 200.0 | 225 | 4.53 | 50.0 |
| 4.001 | 9 | 10 | 9.187 | 0.600 | 54.557 | 54.511 | 0.046 | 200.0 | 225 | 4.70 | 50.0 |
| 1.005 | 10 | 11 | 20.608 | 0.600 | 54.300 | 54.231 | 0.069 | 300.0 | 450 | 8.22 | 50.0 |
| 1.006 | 11 | 13 | 17.699 | 0.600 | 54.156 | 54.097 | 0.059 | 300.0 | 525 | 8.45 | 50.0 |
| 5.000 | 12 | 13 | 9.612 | 0.600 | 54.290 | 54.226 | 0.064 | 150.0 | 225 | 4.15 | 50.0 |
| 1.007 | 13 | 29 | 43.385 | 0.600 | 54.070 | 53.925 | 0.145 | 300.0 | 525 | 9.01 | 50.0 |
| 6.000 | 14 | 15 | 63.002 | 0.600 | 55.770 | 55.350 | 0.420 | 150.0 | 225 | 4.99 | 50.0 |

| Name | Vel (m/s) | Cap (l/s) | Flow (I/s) | US Depth (m) | DS Depth (m) | Σ Area (ha) | Σ Add Inflow (I/s) | Pro Depth (mm) | Pro Velocity (m/s) |
|-------|--------------|--------------|---------------|--------------------|--------------------|----------------|--------------------------|----------------------|--------------------------|
| 1.000 | 1.065 | 42.3 | 16.3 | 0.895 | 1.333 | 0.090 | 0.0 | 96 | 0.995 |
| 1.001 | 0.921 | 36.6 | 33.2 | 1.333 | 1.160 | 0.184 | 0.0 | 169 | 1.040 |
| 2.000 | 1.065 | 42.3 | 21.3 | 1.005 | 1.024 | 0.118 | 0.0 | 113 | 1.067 |
| 1.002 | 1.277 | 141.1 | 80.4 | 1.160 | 0.878 | 0.445 | 0.0 | 203 | 1.318 |
| 3.000 | 0.921 | 36.6 | 33.6 | 1.015 | 0.885 | 0.186 | 0.0 | 170 | 1.040 |
| 1.003 | 1.529 | 168.9 | 147.6 | 0.878 | 1.111 | 0.817 | 0.0 | 273 | 1.714 |
| 1.004 | 1.434 | 228.0 | 158.5 | 1.125 | 1.022 | 0.877 | 0.0 | 277 | 1.544 |
| 4.000 | 0.921 | 36.6 | 10.5 | 0.900 | 1.268 | 0.058 | 0.0 | 82 | 0.796 |
| 4.001 | 0.921 | 36.6 | 21.0 | 1.268 | 1.094 | 0.116 | 0.0 | 122 | 0.950 |
| 1.005 | 1.168 | 185.8 | 190.3 | 1.080 | 1.339 | 1.053 | 0.0 | 383 | 1.320 |
| 1.006 | 1.288 | 278.8 | 201.1 | 1.339 | 1.548 | 1.113 | 0.0 | 331 | 1.397 |
| 5.000 | 1.065 | 42.3 | 10.3 | 1.565 | 1.719 | 0.057 | 0.0 | 75 | 0.880 |
| 1.007 | 1.288 | 278.8 | 229.1 | 1.575 | 0.700 | 1.268 | 0.0 | 364 | 1.430 |
| 6.000 | 1.065 | 42.3 | 148.9 | 1.225 | 1.235 | 0.824 | 0.0 | 225 | 1.085 |

| CAUSEV | | | Waterman | Moylan Con | sulting File: 22-010-SW Network: SW N Paul Donoghue 19/10/2023 | | | | K.pfd F | Page 4 | |
|--------|------------|------------|---------------|----------------|---|--------------|-------------|----------------|-------------|------------------|-----------------|
| | | | | | <u>Lin</u> | <u>ks</u> | | | | | |
| Name | US Node | DS Node | Length (m) | ks (mm) / n | US IL (m) | DS IL (m) | Fall (m) | Slope (1:X) | Dia (mm) | T of C (mins) | Rain (mm/hr) |
| 6.001 | 15 | 16 | 3.471 | 0.600 | 55.275 | 55.236 | 0.039 | 89.0 | 300 | 5.02 | 50.0 |
| 6.002 | 16 | 18 | 33.518 | 0.600 | 55.086 | 54.918 | 0.168 | 199.5 | 450 | 5.41 | 50.0 |
| 7.000 | 17 | 18 | 26.419 | 0.600 | 55.400 | 55.106 | 0.294 | 90.0 | 225 | 4.32 | 50.0 |
| 6.003 | 18 | 19 | 23.049 | 0.600 | 54.918 | 54.826 | 0.092 | 250.5 | 375 | 5.75 | 50.0 |
| 6.004 | 19 | 24 | 33.634 | 0.600 | 54.751 | 54.639 | 0.112 | 300.0 | 450 | 6.23 | 50.0 |
| 8.000 | 20 | 21 | 35.562 | 0.600 | 56.175 | 55.464 | 0.711 | 50.0 | 225 | 4.32 | 50.0 |
| 8.001 | 21 | 23 | 45.337 | 0.600 | 55.464 | 55.011 | 0.453 | 100.0 | 225 | 4.90 | 50.0 |
| 9.000 | 22 | 23 | 34.693 | 0.600 | 55.815 | 55.642 | 0.173 | 200.0 | 300 | 4.52 | 50.0 |
| 8.002 | 23 | 24 | 56.973 | 0.600 | 54.861 | 54.576 | 0.285 | 200.0 | 375 | 5.64 | 50.0 |
| 6.005 | 24 | 25 | 12.795 | 0.600 | 54.190 | 54.147 | 0.043 | 300.0 | 450 | 6.41 | 50.0 |
| 6.006 | 25 | 26 | 36.722 | 0.600 | 54.155 | 54.033 | 0.122 | 300.0 | 450 | 6.93 | 50.0 |
| 6.007 | 26 | 27 | 19.268 | 0.600 | 54.033 | 53.969 | 0.064 | 300.0 | 375 | 7.24 | 50.0 |
| 6.008 | 27 | 29 | 18.542 | 0.600 | 53.969 | 53.907 | 0.062 | 300.0 | 450 | 7.51 | 50.0 |
| 10.000 | 28 | 29 | 15.801 | 0.600 | 55.075 | 54.285 | 0.790 | 20.0 | 225 | 4.09 | 50.0 |
| 1.008 | 29 | 39 | 23.382 | 0.600 | 53.910 | 53.832 | 0.078 | 300.0 | 375 | 9.39 | 50.0 |
| 11.000 | 30 | 31 | 70.058 | 0.600 | 55.900 | 55.433 | 0.467 | 150.0 | 225 | 5.10 | 50.0 |
| 11.001 | 31 | 32 | 9.716 | 0.600 | 55.208 | 55.159 | 0.049 | 200.0 | 450 | 5.21 | 50.0 |
| 11.002 | 32 | 33 | 22.270 | 0.600 | 55.159 | 54.714 | 0.445 | 50.0 | 450 | 5.34 | 50.0 |
| 11.003 | 33 | 36 | 19.444 | 0.600 | 54.714 | 54.617 | 0.097 | 200.0 | 450 | 5.56 | 50.0 |
| 12.000 | 34 | 35 | 22.932 | 0.600 | 55.650 | 55.535 | 0.115 | 200.0 | 225 | 4.42 | 50.0 |
| 12.001 | 35 | 36 | 7.480 | 0.600 | 55.535 | 55.498 | 0.037 | 202.2 | 225 | 4.55 | 50.0 |
| 11.004 | 36 | 38 | 38.107 | 0.600 | 54.429 | 54.302 | 0.127 | 300.1 | 525 | 6.06 | 50.0 |
| 13.000 | 37 | 38 | 58.799 | 0.600 | 55.209 | 54.493 | 0.716 | 82.1 | 225 | 4.68 | 50.0 |
| 11.005 | 38 | 39 | 20.714 | 0.600 | 54.302 | 54.233 | 0.069 | 300.0 | 450 | 6.35 | 50.0 |

| Nam | e Vel | Сар | Flow | US | DS | Σ Area | Σ Add | Pro | Pro |
|-------|---------|-------|-------|-------|-------|--------|--------|-------|----------|
| | (m/s) | (I/s) | (I/s) | Depth | Depth | (ha) | Inflow | Depth | Velocity |
| | | | | (m) | (m) | | (I/s) | (mm) | (m/s) |
| 6.003 | 1.667 | 117.8 | 163.7 | 1.235 | 1.364 | 0.906 | 0.0 | 300 | 1.688 |
| 6.002 | 1.435 | 228.3 | 163.7 | 1.364 | 1.382 | 0.906 | 0.0 | 283 | 1.555 |
| 7.000 | 1.379 | 54.8 | 3.6 | 1.275 | 1.419 | 0.020 | 0.0 | 39 | 0.787 |
| 6.003 | 1.140 | 125.9 | 182.7 | 1.457 | 1.349 | 1.011 | 0.0 | 375 | 1.155 |
| 6.004 | 1.168 | 185.8 | 335.9 | 1.349 | 1.771 | 1.859 | 0.0 | 450 | 1.183 |
| 8.000 | 1.854 | 73.7 | 4.0 | 1.200 | 1.761 | 0.022 | 0.0 | 36 | 1.002 |
| 8.001 | 1.307 | 52.0 | 18.4 | 1.761 | 1.904 | 0.102 | 0.0 | 93 | 1.200 |
| 9.000 | 1.108 | 78.3 | 21.3 | 1.125 | 1.198 | 0.118 | 0.0 | 106 | 0.946 |
| 8.002 | 1.277 | 141.1 | 78.1 | 1.904 | 1.909 | 0.432 | 0.0 | 200 | 1.309 |
| 6.005 | 1.168 | 185.8 | 452.8 | 2.220 | 2.403 | 2.506 | 0.0 | 450 | 1.183 |
| 6.006 | 1.168 | 185.8 | 452.8 | 2.395 | 0.667 | 2.506 | 0.0 | 450 | 1.183 |
| 6.007 | 1.041 | 114.9 | 452.8 | 0.742 | 0.806 | 2.506 | 0.0 | 375 | 1.054 |
| 6.008 | 3 1.168 | 185.8 | 452.8 | 0.731 | 0.793 | 2.506 | 0.0 | 450 | 1.183 |
| 10.00 | 2.939 | 116.8 | 10.3 | 1.700 | 0.640 | 0.057 | 0.0 | 45 | 1.837 |
| 1.008 | 3 1.041 | 114.9 | 702.6 | 0.865 | 0.943 | 3.888 | 0.0 | 375 | 1.054 |
| 11.00 | | 42.3 | 15.0 | 0.705 | 1.792 | 0.083 | 0.0 | 93 | 0.977 |
| 11.00 | - | 228.0 | 165.3 | 1.792 | 1.991 | 0.915 | 0.0 | 285 | 1.557 |
| 11.00 | | 458.1 | 165.3 | 1.991 | 1.886 | 0.915 | 0.0 | 187 | 2.658 |
| 11.00 | | 228.0 | 172.6 | 1.886 | 1.793 | 0.955 | 0.0 | 294 | 1.570 |
| 12.00 | | 36.6 | 5.1 | 1.145 | 1.070 | 0.028 | 0.0 | 57 | 0.652 |
| 12.00 | | 36.4 | 10.1 | 1.070 | 1.137 | 0.056 | 0.0 | 81 | 0.788 |
| 11.00 | | 278.7 | 199.0 | 1.906 | 1.583 | 1.101 | 0.0 | 329 | 1.393 |
| 13.00 | | 57.4 | 9.8 | 1.266 | 1.692 | 0.054 | 0.0 | 63 | 1.085 |
| 11.00 | 1.168 | 185.8 | 219.7 | 1.658 | 0.467 | 1.216 | 0.0 | 450 | 1.183 |
| | | | | | | | | | |

| CAUSE | | | Waterman | Moylan Cor | nsulting | Networ | k: SW NE | -NETWOR ETWORK | K.pfd | Page 5 | | | |
|--------|------------|------------|---------------|-----------------------|--------------|----------------|------------------|-------------------|-------------|------------------|-----------------|--|--|
| | | Links | | | | | | | | | | | |
| Name | US Node | DS Node | Length (m) | ks (mm) / n | US IL (m) | DS IL (m) | Fall (m) | Slope (1:X) | Dia (mm) | T of C (mins) | Rain (mm/hr) | | |
| 1.009 | 39 | 49 | 15.787 | 0.600 | 53.815 | | | | 450 | | 49.8 | | |
| 14.000 | 40 | 41 | 34.884 | 0.600 | 54.825 | 54.653 | 1 0.174 | 200.0 | 225 | 4.63 | 50.0 | | |
| 14.001 | 41 | 42 | 7.097 | 0.600 | 54.325 | 54.290 | 0.035 | 200.0 | 225 | 4.76 | 50.0 | | |
| 14.002 | 42 | 43 | 31.617 | 0.600 | 54.290 | 54.132 | 2 0.158 | 200.0 | 225 | 5.33 | 50.0 | | |
| 14.003 | 43 | 44 | 18.928 | 0.600 | 54.132 | 54.037 | 7 0.095 | 200.0 | 225 | 5.67 | 50.0 | | |
| 14.004 | 44 | 45 | 26.922 | 0.600 | 53.962 | 53.854 | 4 0.108 | 250.0 | 300 | 6.13 | 50.0 | | |
| 14.005 | 45 | 46 | 60.186 | 0.600 | 53.854 | 53.613 | 0.24 1 | 250.0 | 300 | 7.14 | 50.0 | | |
| 14.006 | 46 | 48 | 6.202 | 0.600 | 53.613 | 53.588 | 8 0.025 | 250.0 | 300 | 7.25 | 50.0 | | |
| 15.000 | 47 | 48 | 24.021 | 0.600 | 54.875 | 54.395 | 5 0.480 | 50.0 | 225 | 4.22 | 50.0 | | |
| 14.007 | 48 | 49 | 8.500 | 0.600 | 53.839 | 53.805 | 5 0.034 | 250.0 | 375 | 7.37 | 50.0 | | |
| 1.010 | 49 | 57 | 3.349 | 0.600 | 53.770 | 53.759 | 9 0.011 | 300.0 | 450 | 9.66 | 49.6 | | |
| 16.000 | 50 | 51 | 58.645 | 0.600 | 55.365 | 55.072 | 0.293 | 200.0 | 225 | 5.06 | 50.0 | | |
| 16.001 | 51 | 53 | 30.147 | 0.600 | 55.072 | 54.87 2 | 1 0.201 | 150.0 | 225 | 5.53 | 50.0 | | |
| 17.000 | 52 | 53 | 49.518 | 0.600 | 55.150 | 54.902 | 0.248 | 200.0 | 225 | 4.90 | 50.0 | | |
| 16.002 | 53 | 54 | 59.934 | 0.600 | 54.796 | 54.596 | 6 0. 20 0 | 300.0 | 300 | 6.64 | 50.0 | | |
| 16.003 | 54 | 56 | 24.943 | 0.600 | 54.596 | 54.513 | 0.083 | 300.0 | 300 | 7.10 | 50.0 | | |
| 18.000 | 55 | 56 | 45.393 | 0.600 | 55.275 | 55.048 | 8 0.227 | 200.0 | 225 | 4.82 | 50.0 | | |
| 16.004 | 56 | 57 | 10.102 | 0.600 | 54.438 | 54.387 | 7 0.051 | 200.0 | 375 | | 50.0 | | |
| 1.011 | 57 | 58 | 13.370 | 0.600 | 53.760 | 53.71 | 5 0.045 | 300.0 | 450 | 9.85 | 49.2 | | |
| 1.012 | 58 | 59 | 38.339 | 0.600 | 54.825 | | | | 375 | | 47.8 | | |
| 1.013 | 59 | 60 | 9.851 | 0.600 | 54.685 | | | | 450 | | 47.4 | | |
| 1.014 | 60 | 84 | 16.013 | 0.600 | 54.600 | | | | 450 | | 47.3 | | |
| 19.000 | | 63 | 27.740 | 0.600 | 55.985 | | | | 225 | | 50.0 | | |
| 20.000 | 62 | 63 | 22.338 | 0.600 | 56.170 | 55.772 | 1 0.399 | 56.0 | 225 | 4.21 | 50.0 | | |
| | Name | | • | Flow | US | - | Σ Area | Σ Add | Pro | Pro | | | |
| | | (m/ | ′s) (I/s) | (I/s) | - | Depth | (ha) | Inflow | Depth | Velocity | | | |
| | | | | • • • • | (m) | (m) | | (I/s) | (mm) | (m/s) | | | |
| | 1.009 | | | 917.8 | 0.885 | 2.358 | 5.104 | 0.0 | 450 | 1.183 | | | |
| | 14 00 | 0 0 92 | 21 36.6 | 10 5 | 0 700 | 0 874 | 0.058 | 0.0 | 82 | 0 796 | | | |

| | (m/s) | (I/s) | (I/s) | Depth | Depth | (ha) | Inflow | Depth | Velocity | |
|--------|-------|-------|--------|-------|-------|-------|--------|-------|----------|--|
| | | | | (m) | (m) | | (I/s) | (mm) | (m/s) | |
| 1.009 | 1.168 | 185.8 | 917.8 | 0.885 | 2.358 | 5.104 | 0.0 | 450 | 1.183 | |
| 14.000 | 0.921 | 36.6 | 10.5 | 0.700 | 0.874 | 0.058 | 0.0 | 82 | 0.796 | |
| 14.001 | 0.921 | 36.6 | 21.0 | 1.200 | 1.535 | 0.116 | 0.0 | 122 | 0.950 | |
| 14.002 | 0.921 | 36.6 | 26.2 | 1.535 | 1.703 | 0.145 | 0.0 | 141 | 0.999 | |
| 14.003 | 0.921 | 36.6 | 31.4 | 1.703 | 1.978 | 0.174 | 0.0 | 161 | 1.032 | |
| 14.004 | 0.990 | 70.0 | 39.8 | 1.978 | 2.476 | 0.220 | 0.0 | 162 | 1.020 | |
| 14.005 | 0.990 | 70.0 | 49.9 | 2.476 | 2.487 | 0.276 | 0.0 | 188 | 1.072 | |
| 14.006 | 0.990 | 70.0 | 60.4 | 2.487 | 2.562 | 0.334 | 0.0 | 216 | 1.109 | |
| 15.000 | 1.854 | 73.7 | 10.5 | 1.200 | 1.830 | 0.058 | 0.0 | 57 | 1.317 | |
| 14.007 | 1.141 | 126.0 | 70.8 | 2.236 | 2.390 | 0.392 | 0.0 | 201 | 1.173 | |
| 1.010 | 1.168 | 185.8 | 986.0 | 2.350 | 2.511 | 5.496 | 0.0 | 450 | 1.183 | |
| 16.000 | 0.921 | 36.6 | 14.1 | 1.200 | 1.903 | 0.078 | 0.0 | 97 | 0.863 | |
| 16.001 | 1.065 | 42.3 | 28.2 | 1.903 | 1.934 | 0.156 | 0.0 | 134 | 1.137 | |
| 17.000 | 0.921 | 36.6 | 9.9 | 1.315 | 1.903 | 0.055 | 0.0 | 80 | 0.783 | |
| 16.002 | 0.902 | 63.8 | 46.8 | 1.934 | 1.704 | 0.259 | 0.0 | 191 | 0.983 | |
| 16.003 | 0.902 | 63.8 | 62.2 | 1.704 | 1.887 | 0.344 | 0.0 | 241 | 1.023 | |
| 18.000 | 0.921 | 36.6 | 15.4 | 1.200 | 1.427 | 0.085 | 0.0 | 102 | 0.881 | |
| 16.004 | 1.277 | 141.1 | 92.9 | 1.887 | 1.958 | 0.514 | 0.0 | 222 | 1.360 | |
| 1.011 | 1.168 | 185.8 | 1068.1 | 2.510 | 1.575 | 6.010 | 0.0 | 450 | 1.183 | |
| 1.012 | 1.041 | 114.9 | 1037.4 | 0.540 | 0.678 | 6.010 | 0.0 | 375 | 1.054 | |
| 1.013 | 1.168 | 185.8 | 1030.6 | 0.615 | 1.798 | 6.010 | 0.0 | 450 | 1.183 | |
| 1.014 | 3.180 | 505.7 | 1026.6 | 1.850 | 1.920 | 6.010 | 0.0 | 450 | 3.220 | |
| 19.000 | 0.921 | 36.6 | 10.5 | 1.200 | 1.539 | 0.058 | 0.0 | 82 | 0.796 | |
| 20.000 | 1.751 | 69.6 | 16.8 | 1.005 | 1.614 | 0.093 | 0.0 | 75 | 1.449 | |
| | | | | | | | | | | |

| AUSEV | | | aterman | Moylan Cor | nsulting | Networ | k: SW Ni noghue | -NETWOF ETWORK | K.pfd | Page 6 | | |
|--------|------------|------------|---------------|----------------|--------------|--------------|--------------------|-------------------|-------------|------------------|-----------------|--|
| | | | | | Lin | <u>ks</u> | | | | | | |
| Name | US Node | DS Node | Length (m) | ks (mm) / n | US IL (m) | DS IL (m) | Fall (m) | Slope (1:X) | Dia (mm) | T of C (mins) | Rain (mm/hr) | |
| 19.001 | 63 | 64 | 29.145 | 0.600 | 55.771 | 55.382 | | | 225 | | 50.0 | |
| 19.002 | 64 | 65 | 11.999 | 0.600 | 55.307 | 55.247 | 7 0.060 | 200.0 | 300 | 5.00 | 50.0 | |
| 19.003 | 65 | 68 | 39.685 | 0.600 | 55.247 | 55.049 | 0.198 | 3 200.0 | 300 | 5.60 | 50.0 | |
| 21.000 | 66 | 67 | 58.609 | 0.600 | 55.710 | 55.319 | 9 0.393 | 150.0 | 225 | 4.92 | 50.0 | |
| 21.001 | 67 | 68 | 33.880 | 0.600 | 55.244 | 55.075 | 5 0.169 | 200.5 | 300 | 5.43 | 50.0 | |
| 19.004 | 68 | 69 | 25.057 | 0.600 | 54.974 | 54.849 | 9 0.125 | 200.0 | 375 | 5.93 | 50.0 | |
| 19.005 | 69 | 70 | 19.401 | 0.600 | 54.849 | 54.784 | 4 0.065 | 300.0 | 375 | 6.24 | 50.0 | |
| 19.006 | 70 | 73 | 10.907 | 0.600 | 54.709 | 54.673 | 0.036 | 300.0 | 450 | 6.39 | 50.0 | |
| 22.000 | 71 | 72 | 18.649 | 0.600 | 55.675 | 55.489 | 9 0.186 | 5 100.0 | 225 | 4.24 | 50.0 | |
| 22.001 | 72 | 73 | 49.328 | 0.600 | 55.489 | 54.996 | 5 0.49 3 | 3 100.0 | 225 | 4.87 | 50.0 | |
| 19.007 | 73 | 74 | 12.581 | 0.600 | 54.673 | 54.631 | 1 0.042 | | 450 | 6.57 | 50.0 | |
| 19.008 | 74 | 80 | 16.849 | 0.600 | 54.631 | 54.575 | 5 0.056 | 5 300.0 | 450 | 6.81 | 50.0 | |
| 23.000 | 75 | 77 | 42.182 | 0.600 | 55.090 | 54.879 | 9 0.21 | 200.0 | 300 | 4.63 | 50.0 | |
| 24.000 | 76 | 77 | 34.708 | 0.600 | 55.770 | 55.596 | 5 0.17 4 | 200.0 | 225 | 4.63 | 50.0 | |
| 23.001 | 77 | 78 | 52.984 | 0.600 | 54.870 | 54.693 | 0.17 | 7 300.0 | 375 | 5.48 | 50.0 | |
| 23.002 | 78 | 79 | 12.774 | 0.600 | 54.630 | 54.587 | 7 0.04 3 | 300.0 | 375 | 5.69 | 50.0 | |
| 23.003 | 79 | 80 | 25.689 | 0.600 | 54.587 | 54.501 | 1 0.086 | 5 298.7 | 375 | 6.10 | 50.0 | |
| 19.009 | 80 | 83 | 16.535 | 0.600 | 54.426 | 54.371 | 1 0.055 | | 450 | 7.05 | 50.0 | |
| 25.000 | 81 | 82 | 43.897 | 0.600 | 55.875 | 54.997 | 7 0.878 | 3 50.0 | 225 | 4.39 | 50.0 | |
| 25.001 | 82 | 83 | 30.805 | 0.600 | 54.997 | 54.843 | 0.15 4 | 4 200.0 | 225 | 4.95 | 50.0 | |
| 19.010 | 83 | 84 | 10.838 | 0.600 | 54.265 | 54.229 | 9 0.036 | 5 300.0 | 450 | 7.21 | 50.0 | |
| 1.015 | 84 | 85 | 27.827 | 0.600 | 54.210 | 54.117 | 7 0.09 3 | 300.0 | 300 | 11.20 | 46.2 | |
| 1.016 | 85 | 86 | 11.984 | 0.600 | 54.110 | 54.070 | 0.040 | 300.0 | 300 | 11.42 | 45.7 | |
| 1.017 | 86 | 87 | 38.165 | 0.600 | 54.070 | 53.943 | 3 0.127 | 300.0 | 300 | 12.13 | 44.4 | |
| | Name | | Сар | Flow | US | | Σ Area | Σ Add | Pro | Pro | | |
| | | (m/s) |) (I/s) | (I/s) | | Depth | (ha) | Inflow | Depth | Velocity | | |
| | 40.00 | | | | (m) | (m) | | (I/s) | (mm) | (m/s) | | |
| | 19.00 | | | 44.1 | 1.614 | 1.563 | 0.244 | 0.0 | 144 | 1.648 | | |
| | 19.00 | | | 51.9 | 1.563 | 1.633 | 0.287 | 0.0 | 178 | 1.181 | | |
| | 19.003 | | | 59.6 | 1.633 | 1.401 | 0.330 | 0.0 | 197 | 1.216 | | |
| | 21.00 | | | 14.1 | 1.175 | 1.256 | 0.078 | 0.0 | 89 125 | 0.960 | | |
| | 21.00 | | | | 1.256 | 1.375 | 0.156 | 0.0 | 125 | 1.020 | | |
| | 19.004 | | | 102.5 | 1.401 | 1.576 | 0.567 | 0.0 | 238 | 1.388 | | |
| | 19.00 | | | 110.2 | 1.576 | 1.641 | 0.610 | 0.0 | 296 272 | 1.178 | | |
| | 19.00 | | | 125.6 | 1.641 | 1.577 | 0.695 | 0.0 | 272 | 1.251 | | |
| | 22.00 | | | 7.8 15 5 | 1.200 | 1.386 | 0.043 | 0.0 | 58 84 | 0.944 | | |
| | 22.00 | | | 15.5 | 1.386 | 1.479 | 0.086 | 0.0 | 84 | 1.143 | | |
| | 19.00 | | | 148.9 | 1.577 | 1.619 | 0.824 | 0.0 | 306 | 1.293 | | |
| | 19.00 | | | 148.9 | | 0.975 | 0.824 | 0.0 | 306 | 1.293 | | |
| | 23.00 | | | 21.5 | | 2.441 | 0.119 | 0.0 | 107 | 0.948 | | |
| | 24.00 | | | 8.3 | 1.025 | 1.799 | 0.046 | 0.0 | 73 | 0.747 | | |
| | 23.00 | | | 45.2 | 2.375 | 1.932 | 0.250 | 0.0 | 163 | 0.980 | | |
| | 23.00 | | | 45.2 | | 1.038 | 0.250 | 0.0 | 163 | 0.980 | | |
| | 23.003 | | | | | 1.124 | 0.280 | 0.0 | 174 | 1.011 | | |
| | 19.009 | 9 1.167 | 185.6 | 204.9 | 1.124 | 2.039 | 1.134 | 0.0 | 450 | 1.182 | | |

1.778

1.792

1.901

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25.000 1.854

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0.902

25.001

1.015

1.016

1.017

| CAUSE | WAY | - | Waterman M | loylan Consu | N P | File: 22-010-SW-NETWORK.pfdPage 7Network: SW NETWORKPaul Donoghue19/10/202319/10/2023 | | | | | |
|--------|------------|------------|---------------|----------------|--------------|---|-------------|----------------|-------------|------------------|-----------------|
| | | | | | <u>Links</u> | | | | | | |
| Name | US Node | DS Node | Length (m) | ks (mm) / n | US IL (m) | DS IL (m) | Fall (m) | Slope (1:X) | Dia (mm) | T of C (mins) | Rain (mm/hr) |
| 1.018 | 87 | 88 | 7.294 | 0.600 | 53.943 | 53.919 | 0.024 | 300.0 | 300 | 12.26 | (1111) |
| 1.010 | 88 | 107 | 82.343 | 0.600 | 53.919 | 53.645 | 0.274 | 300.0 | 300 | 13.78 | 41.5 |
| 26.000 | 89 | 90 | 19.890 | 0.600 | 55.955 | 55.856 | 0.099 | 200.0 | 225 | 4.36 | 50.0 |
| 26.001 | 90 | 92 | 33.584 | 0.600 | 55.856 | 55.688 | 0.168 | 200.0 | 225 | 4.97 | 50.0 |
| 27.000 | 91 | 92 | 25.331 | 0.600 | 57.425 | 56.792 | 0.633 | 40.0 | 225 | 4.20 | 50.0 |
| 26.002 | 92 | 93 | 24.854 | 0.600 | 55.688 | 55.510 | 0.178 | 140.0 | 225 | 5.34 | 50.0 |
| 26.003 | 93 | 95 | 39.554 | 0.600 | 55.510 | 55.114 | 0.396 | 100.0 | 225 | 5.85 | 50.0 |
| 28.000 | 94 | 95 | 17.416 | 0.600 | 55.570 | 55.483 | 0.087 | 200.0 | 225 | 4.32 | 50.0 |
| 26.004 | 95 | 96 | 26.758 | 0.600 | 54.470 | 54.381 | 0.089 | 300.7 | 450 | 6.23 | 50.0 |
| 26.005 | 96 | 97 | 30.915 | 0.600 | 54.381 | 54.278 | 0.103 | 300.1 | 450 | 6.67 | 50.0 |
| 26.006 | 97 | 98 | 4.319 | 0.600 | 54.278 | 54.264 | 0.014 | 300.0 | 450 | 6.73 | 50.0 |
| 26.007 | 98 | 99 | 49.445 | 0.600 | 54.264 | 54.099 | 0.165 | 300.0 | 450 | 7.44 | 50.0 |
| 26.008 | 99 | 100 | 31.884 | 0.600 | 54.099 | 53.993 | 0.106 | 300.0 | 450 | 7.89 | 50.0 |
| 26.009 | 100 | 102 | 33.969 | 0.600 | 53.993 | 53.880 | 0.113 | 300.0 | 450 | 8.38 | 50.0 |
| 29.000 | 101 | 102 | 98.766 | 0.600 | 57.775 | 54.483 | 3.292 | 30.0 | 225 | 4.69 | 50.0 |
| 26.010 | 102 | 105 | 5.644 | 0.600 | 53.805 | 53.786 | 0.019 | 300.0 | 525 | 8.45 | 50.0 |
| 30.000 | 103 | 104 | 57.308 | 0.600 | 54.875 | 54.493 | 0.382 | 150.0 | 225 | 4.90 | 50.0 |
| 30.001 | 104 | 105 | 21.225 | 0.600 | 54.493 | 54.352 | 0.141 | 150.0 | 225 | 5.23 | 50.0 |
| 26.011 | 105 | 106 | 4.776 | 0.600 | 53.786 | 53.770 | 0.016 | 300.0 | 525 | 8.51 | 50.0 |
| 26.012 | 106 | 107 | 12.416 | 0.600 | 53.770 | 53.729 | 0.041 | 300.0 | 525 | 8.67 | 50.0 |
| 1.020 | 107 | 107_OL | JT 19.717 | 0.600 | 53.645 | 53.579 | 0.066 | 300.0 | 300 | 14.15 | 41.0 |

| Name | Vel (m/s) | Cap (I/s) | Flow (I/s) | US Depth (m) | DS Depth (m) | Σ Area (ha) | Σ Add Inflow (I/s) | Pro Depth (mm) | Pro Velocity (m/s) |
|--------|--------------|--------------|---------------|--------------------|--------------------|----------------|--------------------------|----------------------|--------------------------|
| 1.018 | 0.902 | 63.8 | 1175.9 | 2.657 | 1.411 | 7.373 | 0.0 | 300 | 0.914 |
| 1.019 | 0.902 | 63.8 | 1107.1 | 1.411 | 2.655 | 7.373 | 0.0 | 300 | 0.914 |
| 26.000 | 0.921 | 36.6 | 4.5 | 1.200 | 1.819 | 0.025 | 0.0 | 53 | 0.629 |
| 26.001 | 0.921 | 36.6 | 9.0 | 1.819 | 2.327 | 0.050 | 0.0 | 76 | 0.765 |
| 27.000 | 2.074 | 82.5 | 5.2 | 1.200 | 1.223 | 0.029 | 0.0 | 38 | 1.171 |
| 26.002 | 1.103 | 43.8 | 22.4 | 2.327 | 2.105 | 0.124 | 0.0 | 114 | 1.108 |
| 26.003 | 1.307 | 52.0 | 45.5 | 2.105 | 0.661 | 0.252 | 0.0 | 164 | 1.469 |
| 28.000 | 0.921 | 36.6 | 0.0 | 0.205 | 0.292 | 0.000 | 0.0 | 0 | 0.000 |
| 26.004 | 1.167 | 185.6 | 69.6 | 1.080 | 1.169 | 0.385 | 0.0 | 190 | 1.086 |
| 26.005 | 1.168 | 185.8 | 79.1 | 1.169 | 1.272 | 0.438 | 0.0 | 205 | 1.124 |
| 26.006 | 1.168 | 185.8 | 107.3 | 1.272 | 1.286 | 0.594 | 0.0 | 246 | 1.208 |
| 26.007 | 1.168 | 185.8 | 128.7 | 1.286 | 1.451 | 0.712 | 0.0 | 276 | 1.257 |
| 26.008 | 1.168 | 185.8 | 128.7 | 1.451 | 2.147 | 0.712 | 0.0 | 276 | 1.257 |
| 26.009 | 1.168 | 185.8 | 153.6 | 2.147 | 2.490 | 0.850 | 0.0 | 313 | 1.299 |
| 29.000 | 2.397 | 95.3 | 34.0 | 1.200 | 2.112 | 0.188 | 0.0 | 93 | 2.201 |
| 26.010 | 1.288 | 278.8 | 230.4 | 2.490 | 1.689 | 1.275 | 0.0 | 366 | 1.431 |
| 30.000 | 1.065 | 42.3 | 15.0 | 0.900 | 1.832 | 0.083 | 0.0 | 93 | 0.977 |
| 30.001 | 1.065 | 42.3 | 30.0 | 1.832 | 1.423 | 0.166 | 0.0 | 140 | 1.153 |
| 26.011 | 1.288 | 278.8 | 260.4 | 1.689 | 2.445 | 1.441 | 0.0 | 405 | 1.453 |
| 26.012 | 1.288 | 278.8 | 260.4 | 2.445 | 2.346 | 1.441 | 0.0 | 405 | 1.453 |
| 1.020 | 0.902 | 63.8 | 1305.5 | 2.655 | 2.121 | 8.814 | 0.0 | 300 | 0.914 |



| SEM | | | | | isuning | | - | | | |
|----------------|------------------|----------------|------------|----------------------|------------------|------------------|----------------|------------------|------------------|----------------|
| | | | | | <u>Pipeline</u> | <u>Schedule</u> | | | | |
| Link | Length | Slope | Dia | Link | US CL | US IL | US Depth | DS CL | DS IL | DS Depth |
| 1 000 | (m) | (1:X) | (mm) | Туре | (m) | (m) | (m) | (m) | (m) | (m) |
| 1.000 | 68.660 | 150.0 | 225 | Circular | 57.320 | 56.200 | 0.895 | 57.300 | 55.742 | 1.333 |
| 1.001 | 65.454 | 200.0 | 225 | Circular | 57.300 | 55.742 | 1.333 1.005 | 56.800 | 55.415 | 1.160 |
| 2.000 1.002 | 56.907 67.671 | 150.0 200.0 | 225 375 | Circular Circular | 57.160 56.800 | 55.930 55.265 | 1.005 | 56.800 56.180 | 55.551 54.927 | 1.024 0.878 |
| 3.0002 | 74.011 | 200.0 | 225 | Circular | 56.680 | 55.440 | 1.100 | 56.180 56.180 | 55.070 | 0.878 |
| 1.003 | 57.761 | 140.0 | 375 | Circular | 56.180 | 54.927 | 0.878 | 56.000 | 54.514 | 1.111 |
| 1.003 | 13.354 | 200.0 | 450 | Circular | 56.000 | 54.425 | 1.125 | 55.830 | 54.358 | 1.022 |
| 4.000 | 29.534 | 200.0 | 225 | Circular | 55.830 | 54.705 | 0.900 | 56.050 | 54.557 | 1.268 |
| 4.001 | 9.187 | 200.0 | 225 | Circular | 56.050 | 54.557 | 1.268 | 55.830 | 54.511 | 1.094 |
| 1.005 | 20.608 | 300.0 | 450 | Circular | 55.830 | 54.300 | 1.080 | 56.020 | 54.231 | 1.339 |
| 1.006 | 17.699 | 300.0 | 525 | Circular | 56.020 | 54.156 | 1.339 | 56.170 | 54.097 | 1.548 |
| 5.000 | 9.612 | 150.0 | 225 | Circular | 56.080 | 54.290 | 1.565 | 56.170 | 54.226 | 1.719 |
| 1.007 | 43.385 | 300.0 | 525 | Circular | 56.170 | 54.070 | 1.575 | 55.150 | 53.925 | 0.700 |
| 6.000 | 63.002 | 150.0 | 225 | Circular | 57.220 | 55.770 | 1.225 | 56.810 | 55.350 | 1.235 |
| 6.001 | 3.471 | 89.0 | 300 | Circular | 56.810 | 55.275 | 1.235 | 56.900 | 55.236 | 1.364 |
| 6.002 | 33.518 | 199.5 | 450 | Circular | 56.900 | 55.086 | 1.364 | 56.750 | 54.918 | 1.382 |
| 7.000 | 26.419 | 90.0 | 225 | Circular | 56.900 | 55.400 | 1.275 | 56.750 | 55.106 | 1.419 |
| 6.003 | 23.049 | 250.5 | 375 | Circular | 56.750 | 54.918 | 1.457 | 56.550 | 54.826 | 1.349 |
| 6.004 | 33.634 | 300.0 | 450 | Circular | 56.550 | 54.751 | 1.349 | 56.860 | 54.639 | 1.771 |
| 8.000 | 35.562 | 50.0 | 225 | Circular | 57.600 | 56.175 | 1.200 | 57.450 | 55.464 | 1.761 |
| 8.001 | 45.337 | 100.0 | 225 | Circular | 57.450 | 55.464 | 1.761 | 57.140 | 55.011 | 1.904 |
| 9.000 | 34.693 | 200.0 | 300 | Circular | 57.240 | 55.815 | 1.125 | 57.140 | 55.642 | 1.198 |
| 8.002 | 56.973 | 200.0 | 375 | Circular | 57.140 | 54.861 | 1.904 | 56.860 | 54.576 | 1.909 |
| 6.005 | 12.795 | 300.0 | 450 | Circular | 56.860 | 54.190 | 2.220 | 57.000 | 54.147 | 2.403 |
| 6.006 | 36.722 | 300.0 | 450 | Circular | 57.000 | 54.155 | 2.395 | 55.150 | 54.033 | 0.667 |
| | | | | | | | | | | |

File: 22-010-SW-NETWORK.pfd Page 8

Waterman Moylan Consulting

| Link | US | Dia | Node | МН | DS | Dia | Node | МН |
|-------|------|------|---------|-----------|------|------|---------|-----------|
| | Node | (mm) | Туре | Туре | Node | (mm) | Туре | Туре |
| 1.000 | 1 | 1200 | Manhole | Adoptable | 2 | 1200 | Manhole | Adoptable |
| 1.001 | 2 | 1200 | Manhole | Adoptable | 4 | 1200 | Manhole | Adoptable |
| 2.000 | 3 | 1200 | Manhole | Adoptable | 4 | 1200 | Manhole | Adoptable |
| 1.002 | 4 | 1200 | Manhole | Adoptable | 6 | 1200 | Manhole | Adoptable |
| 3.000 | 5 | 1200 | Manhole | Adoptable | 6 | 1200 | Manhole | Adoptable |
| 1.003 | 6 | 1200 | Manhole | Adoptable | 7 | 1350 | Manhole | Adoptable |
| 1.004 | 7 | 1350 | Manhole | Adoptable | 10 | 1200 | Manhole | Adoptable |
| 4.000 | 8 | 1200 | Manhole | Adoptable | 9 | 1200 | Manhole | Adoptable |
| 4.001 | 9 | 1200 | Manhole | Adoptable | 10 | 1200 | Manhole | Adoptable |
| 1.005 | 10 | 1200 | Manhole | Adoptable | 11 | 1200 | Manhole | Adoptable |
| 1.006 | 11 | 1200 | Manhole | Adoptable | 13 | 1200 | Manhole | Adoptable |
| 5.000 | 12 | 1200 | Manhole | Adoptable | 13 | 1200 | Manhole | Adoptable |
| 1.007 | 13 | 1200 | Manhole | Adoptable | 29 | 1200 | Manhole | Adoptable |
| 6.000 | 14 | 1200 | Manhole | Adoptable | 15 | 1200 | Manhole | Adoptable |
| 6.001 | 15 | 1200 | Manhole | Adoptable | 16 | 1200 | Manhole | Adoptable |
| 6.002 | 16 | 1200 | Manhole | Adoptable | 18 | 1200 | Manhole | Adoptable |
| 7.000 | 17 | 1200 | Manhole | Adoptable | 18 | 1200 | Manhole | Adoptable |
| 6.003 | 18 | 1200 | Manhole | Adoptable | 19 | 1200 | Manhole | Adoptable |
| 6.004 | 19 | 1200 | Manhole | Adoptable | 24 | 1200 | Manhole | Adoptable |
| 8.000 | 20 | 1200 | Manhole | Adoptable | 21 | 1200 | Manhole | Adoptable |
| 8.001 | 21 | 1200 | Manhole | Adoptable | 23 | 1200 | Manhole | Adoptable |
| 9.000 | 22 | 1200 | Manhole | Adoptable | 23 | 1200 | Manhole | Adoptable |
| 8.002 | 23 | 1200 | Manhole | Adoptable | 24 | 1200 | Manhole | Adoptable |
| 6.005 | 24 | 1200 | Manhole | Adoptable | 25 | 1200 | Manhole | Adoptable |
| 6.006 | 25 | 1200 | Manhole | Adoptable | 26 | 1200 | Manhole | Adoptable |
| | | | | | | | | |



| | | Wate | erman M | oylan Con | sulting | File: 22-0 | 10-SW-NETV | VORK.pfd | Page 9 | | | |
|--------|--------|-------|---------|-----------|------------|------------|------------|----------|--------|----------|--|--|
| | | | | | | Network: | SW NETWO | RK | | | | |
| | | | | | | Paul Don | oghue | | | | | |
| | | | | | | 19/10/20 | 23 | | | | | |
| | | | | | Pipeline S | | | | | | | |
| | | | | <u>I</u> | | | | | | | | |
| Link | Length | Slope | Dia | Link | US CL | US IL | US Depth | DS CL | DS IL | DS Depth | | |
| | (m) | (1:X) | (mm) | Туре | (m) | (m) | (m) | (m) | (m) | (m) | | |
| 6.007 | 19.268 | 300.0 | 375 | Circular | 55.150 | 54.033 | 0.742 | 55.150 | 53.969 | 0.806 | | |
| 6.008 | 18.542 | 300.0 | 450 | Circular | 55.150 | 53.969 | 0.731 | 55.150 | 53.907 | 0.793 | | |
| 10.000 | 15.801 | 20.0 | 225 | Circular | 57.000 | 55.075 | 1.700 | 55.150 | 54.285 | 0.640 | | |
| 1.008 | 23.382 | 300.0 | 375 | Circular | 55.150 | 53.910 | 0.865 | 55.150 | 53.832 | 0.943 | | |
| 11.000 | 70.058 | 150.0 | 225 | Circular | 56.830 | 55.900 | 0.705 | 57.450 | 55.433 | 1.792 | | |
| 11.001 | 9.716 | 200.0 | 450 | Circular | 57.450 | 55.208 | 1.792 | 57.600 | 55.159 | 1.991 | | |
| 11.002 | 22.270 | 50.0 | 450 | Circular | 57.600 | 55.159 | 1.991 | 57.050 | 54.714 | 1.886 | | |
| 11.003 | 19.444 | 200.0 | 450 | Circular | 57.050 | 54.714 | 1.886 | 56.860 | 54.617 | 1.793 | | |
| 12.000 | 22.932 | 200.0 | 225 | Circular | 57.020 | 55.650 | 1.145 | 56.830 | 55.535 | 1.070 | | |
| 12.001 | 7.480 | 202.2 | 225 | Circular | 56.830 | 55.535 | 1.070 | 56.860 | 55.498 | 1.137 | | |
| 11.004 | 38.107 | 300.1 | 525 | Circular | 56.860 | 54.429 | 1.906 | 56.410 | 54.302 | 1.583 | | |
| 13.000 | 58.799 | 82.1 | 225 | Circular | 56.700 | 55.209 | 1.266 | 56.410 | 54.493 | 1.692 | | |
| 11.005 | 20.714 | 300.0 | 450 | Circular | 56.410 | 54.302 | 1.658 | 55.150 | 54.233 | 0.467 | | |
| 1.009 | 15.787 | 300.0 | 450 | Circular | 55.150 | 53.815 | 0.885 | 56.570 | 53.762 | 2.358 | | |
| 14.000 | 34.884 | 200.0 | 225 | Circular | 55.750 | 54.825 | 0.700 | 55.750 | 54.651 | 0.874 | | |
| 14.001 | 7.097 | 200.0 | 225 | Circular | 55.750 | 54.325 | 1.200 | 56.050 | 54.290 | 1.535 | | |
| 14.002 | 31.617 | 200.0 | 225 | Circular | 56.050 | 54.290 | 1.535 | 56.060 | 54.132 | 1.703 | | |
| 14.003 | 18.928 | 200.0 | 225 | Circular | 56.060 | 54.132 | 1.703 | 56.240 | 54.037 | 1.978 | | |
| 14.004 | 26.922 | 250.0 | 300 | Circular | 56.240 | 53.962 | 1.978 | 56.630 | 53.854 | 2.476 | | |
| 14.005 | 60.186 | 250.0 | 300 | Circular | 56.630 | 53.854 | 2.476 | 56.400 | 53.613 | 2.487 | | |
| 14.006 | 6.202 | 250.0 | 300 | Circular | 56.400 | 53.613 | 2.487 | 56.450 | 53.588 | 2.562 | | |
| | | | | | | | | | | | | |

56.450 53.839

56.570 53.770

225 Circular 56.790 55.365

1.200 56.450 54.395

2.350

2.236 56.570 53.805

1.200 57.200 55.072

56.720 53.759

1.830

2.390

2.511

1.903

| Link | US Node | Dia (mm) | Node Type | MH Type | DS Node | Dia (mm) | Node Type | MH Type |
|--------|------------|-------------|--------------|------------|------------|-------------|--------------|------------|
| 6.007 | 26 | 1200 | Manhole | Adoptable | 27 | 1200 | Manhole | Adoptable |
| 6.008 | 27 | 1200 | Manhole | Adoptable | 29 | 1200 | Manhole | Adoptable |
| 10.000 | 28 | 1200 | Manhole | Adoptable | 29 | 1200 | Manhole | Adoptable |
| 1.008 | 29 | 1200 | Manhole | Adoptable | 39 | 1200 | Manhole | Adoptable |
| 11.000 | 30 | 1200 | Manhole | Adoptable | 31 | 1200 | Manhole | Adoptable |
| 11.001 | 31 | 1200 | Manhole | Adoptable | 32 | 1200 | Manhole | Adoptable |
| 11.002 | 32 | 1200 | Manhole | Adoptable | 33 | 1200 | Manhole | Adoptable |
| 11.003 | 33 | 1200 | Manhole | Adoptable | 36 | 1200 | Manhole | Adoptable |
| 12.000 | 34 | 1200 | Manhole | Adoptable | 35 | 1200 | Manhole | Adoptable |
| 12.001 | 35 | 1200 | Manhole | Adoptable | 36 | 1200 | Manhole | Adoptable |
| 11.004 | 36 | 1200 | Manhole | Adoptable | 38 | 1200 | Manhole | Adoptable |
| 13.000 | 37 | 1200 | Manhole | Adoptable | 38 | 1200 | Manhole | Adoptable |
| L1.005 | 38 | 1200 | Manhole | Adoptable | 39 | 1200 | Manhole | Adoptable |
| 1.009 | 39 | 1200 | Manhole | Adoptable | 49 | 1500 | Manhole | Adoptable |
| 14.000 | 40 | 1200 | Manhole | Adoptable | 41 | 1200 | Manhole | Adoptable |
| 14.001 | 41 | 1200 | Manhole | Adoptable | 42 | 1200 | Manhole | Adoptable |
| 14.002 | 42 | 1200 | Manhole | Adoptable | 43 | 1200 | Manhole | Adoptable |
| 14.003 | 43 | 1200 | Manhole | Adoptable | 44 | 1200 | Manhole | Adoptable |
| 14.004 | 44 | 1200 | Manhole | Adoptable | 45 | 1200 | Manhole | Adoptable |
| 14.005 | 45 | 1200 | Manhole | Adoptable | 46 | 1200 | Manhole | Adoptable |
| 14.006 | 46 | 1200 | Manhole | Adoptable | 48 | 1200 | Manhole | Adoptable |
| 15.000 | 47 | 1200 | Manhole | Adoptable | 48 | 1200 | Manhole | Adoptable |
| 14.007 | 48 | 1200 | Manhole | Adoptable | 49 | 1500 | Manhole | Adoptable |
| 1.010 | 49 | 1500 | Manhole | Adoptable | 57 | 1200 | Manhole | Adoptable |
| 16.000 | 50 | 1200 | Manhole | Adoptable | 51 | 1200 | Manhole | Adoptable |

15.000 24.021 50.0 225 Circular 56.300 54.875

375 Circular

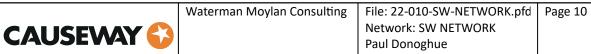
450 Circular

14.007 8.500 250.0

16.000 58.645 200.0

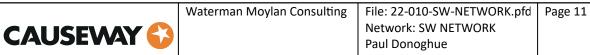
1.010

3.349 300.0



| SEW | | | | , | 0 | Network: Paul Done 19/10/20 | - | | | | |
|--------|---------------|----------------|-------------|--------------|--------------|-----------------------------------|-----------------|--------------|--------------|-----------------|--|
| | | | | <u> </u> | Pipeline S | <u>Schedule</u> | | | | | |
| Link | Length (m) | Slope (1:X) | Dia (mm) | Link Type | US CL (m) | US IL (m) | US Depth (m) | DS CL (m) | DS IL (m) | DS Depth (m) | |
| 16.001 | 30.147 | 150.0 | 225 | Circular | 57.200 | 55.072 | 1.903 | 57.030 | 54.871 | 1.934 | |
| 17.000 | 49.518 | 200.0 | 225 | Circular | 56.690 | 55.150 | 1.315 | 57.030 | 54.902 | 1.903 | |
| 16.002 | 59.934 | 300.0 | 300 | Circular | 57.030 | 54.796 | 1.934 | 56.600 | 54.596 | 1.704 | |
| 16.003 | 24.943 | 300.0 | 300 | Circular | 56.600 | 54.596 | 1.704 | 56.700 | 54.513 | 1.887 | |
| 18.000 | 45.393 | 200.0 | 225 | Circular | 56.700 | 55.275 | 1.200 | 56.700 | 55.048 | 1.427 | |
| 16.004 | 10.102 | 200.0 | 375 | Circular | 56.700 | 54.438 | 1.887 | 56.720 | 54.387 | 1.958 | |
| 1.011 | 13.370 | 300.0 | 450 | Circular | 56.720 | 53.760 | 2.510 | 55.740 | 53.715 | 1.575 | |
| 1.012 | 38.339 | 300.0 | 375 | Circular | 55.740 | 54.825 | 0.540 | 55.750 | 54.697 | 0.678 | |
| 1.013 | 9.851 | 300.0 | 450 | Circular | 55.750 | 54.685 | 0.615 | 56.900 | 54.652 | 1.798 | |
| 1.014 | 16.013 | 41.1 | 450 | Circular | 56.900 | 54.600 | 1.850 | 56.580 | 54.210 | 1.920 | |
| 19.000 | 27.740 | 200.0 | 225 | Circular | 57.410 | 55.985 | 1.200 | 57.610 | 55.846 | 1.539 | |
| 20.000 | 22.338 | 56.0 | 225 | Circular | 57.400 | 56.170 | 1.005 | 57.610 | 55.771 | 1.614 | |
| 19.001 | 29.145 | 75.0 | 225 | Circular | 57.610 | 55.771 | 1.614 | 57.170 | 55.382 | 1.563 | |
| 19.002 | 11.999 | 200.0 | 300 | Circular | 57.170 | 55.307 | 1.563 | 57.180 | 55.247 | 1.633 | |
| 19.003 | 39.685 | 200.0 | 300 | Circular | 57.180 | 55.247 | 1.633 | 56.750 | 55.049 | 1.401 | |
| 21.000 | 58.609 | 150.0 | 225 | Circular | 57.110 | 55.710 | 1.175 | 56.800 | 55.319 | 1.256 | |
| 21.001 | 33.880 | 200.5 | 300 | Circular | 56.800 | 55.244 | 1.256 | 56.750 | 55.075 | 1.375 | |
| 19.004 | 25.057 | 200.0 | 375 | Circular | 56.750 | 54.974 | 1.401 | 56.800 | 54.849 | 1.576 | |
| 19.005 | 19.401 | 300.0 | 375 | Circular | 56.800 | 54.849 | 1.576 | 56.800 | 54.784 | 1.641 | |
| 19.006 | 10.907 | 300.0 | 450 | Circular | 56.800 | 54.709 | 1.641 | 56.700 | 54.673 | 1.577 | |
| 22.000 | 18.649 | 100.0 | 225 | Circular | 57.100 | 55.675 | 1.200 | 57.100 | 55.489 | 1.386 | |
| 22.001 | 49.328 | 100.0 | 225 | Circular | 57.100 | 55.489 | 1.386 | 56.700 | 54.996 | 1.479 | |
| 19.007 | 12.581 | 300.0 | 450 | Circular | 56.700 | 54.673 | 1.577 | 56.700 | 54.631 | 1.619 | |
| 19.008 | 16.849 | 300.0 | 450 | Circular | 56.700 | 54.631 | 1.619 | 56.000 | 54.575 | 0.975 | |
| 23.000 | 42.182 | 200.0 | 300 | Circular | 56.520 | 55.090 | 1.130 | 57.620 | 54.879 | 2.441 | |

| Link | US | Dia | Node | МН | DS | Dia | Node | MH |
|--------|------|------|---------|-----------|------|------|---------|-----------|
| | Node | (mm) | Туре | Туре | Node | (mm) | Туре | Туре |
| 16.001 | 51 | 1200 | Manhole | Adoptable | 53 | 1200 | Manhole | Adoptable |
| 17.000 | 52 | 1200 | Manhole | Adoptable | 53 | 1200 | Manhole | Adoptable |
| 16.002 | 53 | 1200 | Manhole | Adoptable | 54 | 1200 | Manhole | Adoptable |
| 16.003 | 54 | 1200 | Manhole | Adoptable | 56 | 1200 | Manhole | Adoptable |
| 18.000 | 55 | 1200 | Manhole | Adoptable | 56 | 1200 | Manhole | Adoptable |
| 16.004 | 56 | 1200 | Manhole | Adoptable | 57 | 1200 | Manhole | Adoptable |
| 1.011 | 57 | 1200 | Manhole | Adoptable | 58 | 1200 | Manhole | Adoptable |
| 1.012 | 58 | 1200 | Manhole | Adoptable | 59 | 1200 | Manhole | Adoptable |
| 1.013 | 59 | 1200 | Manhole | Adoptable | 60 | 1350 | Manhole | Adoptable |
| 1.014 | 60 | 1350 | Manhole | Adoptable | 84 | 1800 | Manhole | Adoptable |
| 19.000 | 61 | 1200 | Manhole | Adoptable | 63 | 1200 | Manhole | Adoptable |
| 20.000 | 62 | 1200 | Manhole | Adoptable | 63 | 1200 | Manhole | Adoptable |
| 19.001 | 63 | 1200 | Manhole | Adoptable | 64 | 1200 | Manhole | Adoptable |
| 19.002 | 64 | 1200 | Manhole | Adoptable | 65 | 1200 | Manhole | Adoptable |
| 19.003 | 65 | 1200 | Manhole | Adoptable | 68 | 1200 | Manhole | Adoptable |
| 21.000 | 66 | 1200 | Manhole | Adoptable | 67 | 1200 | Manhole | Adoptable |
| 21.001 | 67 | 1200 | Manhole | Adoptable | 68 | 1200 | Manhole | Adoptable |
| 19.004 | 68 | 1200 | Manhole | Adoptable | 69 | 1200 | Manhole | Adoptable |
| 19.005 | 69 | 1200 | Manhole | Adoptable | 70 | 1200 | Manhole | Adoptable |
| 19.006 | 70 | 1200 | Manhole | Adoptable | 73 | 1200 | Manhole | Adoptable |
| 22.000 | 71 | 1200 | Manhole | Adoptable | 72 | 1200 | Manhole | Adoptable |
| 22.001 | 72 | 1200 | Manhole | Adoptable | 73 | 1200 | Manhole | Adoptable |
| 19.007 | 73 | 1200 | Manhole | Adoptable | 74 | 1350 | Manhole | Adoptable |
| 19.008 | 74 | 1350 | Manhole | Adoptable | 80 | 1350 | Manhole | Adoptable |
| 23.000 | 75 | 1200 | Manhole | Adoptable | 77 | 1350 | Manhole | Adoptable |
| | | | | | | | | |



| SEW | AY 🤇 | | Network: SW NETWORK Paul Donoghue 19/10/2023 | | | | | | | |
|--------|---------------|----------------|--|--------------|--------------|-----------------|-----------------|--------------|--------------|-----------------|
| | | | | <u> </u> | Pipeline S | <u>Schedule</u> | | | | |
| Link | Length (m) | Slope (1:X) | Dia (mm) | Link Type | US CL (m) | US IL (m) | US Depth (m) | DS CL (m) | DS IL (m) | DS Depth (m) |
| 24.000 | 34.708 | 200.0 | 225 | Circular | 57.020 | 55.770 | 1.025 | 57.620 | 55.596 | 1.799 |
| 23.001 | 52.984 | 300.0 | 375 | Circular | 57.620 | 54.870 | 2.375 | 57.000 | 54.693 | 1.932 |
| 23.002 | 12.774 | 300.0 | 375 | Circular | 57.000 | 54.630 | 1.995 | 56.000 | 54.587 | 1.038 |
| 23.003 | 25.689 | 298.7 | 375 | Circular | 56.000 | 54.587 | 1.038 | 56.000 | 54.501 | 1.124 |
| 19.009 | 16.535 | 300.6 | 450 | Circular | 56.000 | 54.426 | 1.124 | 56.860 | 54.371 | 2.039 |
| 25.000 | 43.897 | 50.0 | 225 | Circular | 57.000 | 55.875 | 0.900 | 57.000 | 54.997 | 1.778 |
| 25.001 | 30.805 | 200.0 | 225 | Circular | 57.000 | 54.997 | 1.778 | | 54.843 | 1.792 |
| 19.010 | 10.838 | 300.0 | 450 | Circular | 56.860 | 54.265 | 2.145 | | 54.229 | 1.901 |
| 1.015 | 27.827 | 300.0 | 300 | Circular | 56.580 | 54.210 | 2.070 | 56.240 | 54.117 | 1.823 |
| 1.016 | 11.984 | 300.0 | 300 | Circular | 56.240 | 54.110 | 1.830 | 56.020 | 54.070 | 1.650 |
| 1.017 | 38.165 | 300.0 | 300 | Circular | 56.020 | 54.070 | 1.650 | 56.900 | 53.943 | 2.657 |
| 1.018 | 7.294 | 300.0 | 300 | Circular | 56.900 | 53.943 | 2.657 | 55.630 | 53.919 | 1.411 |
| 1.019 | 82.343 | 300.0 | 300 | Circular | 55.630 | 53.919 | 1.411 | 56.600 | 53.645 | 2.655 |
| 26.000 | 19.890 | 200.0 | 225 | Circular | 57.380 | 55.955 | 1.200 | 57.900 | 55.856 | 1.819 |
| 26.001 | 33.584 | 200.0 | 225 | Circular | 57.900 | 55.856 | 1.819 | 58.240 | 55.688 | 2.327 |
| 27.000 | 25.331 | 40.0 | 225 | Circular | 58.850 | 57.425 | 1.200 | 58.240 | 56.792 | 1.223 |
| 26.002 | 24.854 | 140.0 | 225 | Circular | 58.240 | 55.688 | 2.327 | 57.840 | 55.510 | 2.105 |
| 26.003 | 39.554 | 100.0 | 225 | Circular | 57.840 | 55.510 | 2.105 | 56.000 | 55.114 | 0.661 |
| 28.000 | 17.416 | 200.0 | 225 | Circular | 56.000 | 55.570 | 0.205 | 56.000 | 55.483 | 0.292 |
| 26.004 | 26.758 | 300.7 | 450 | Circular | 56.000 | 54.470 | 1.080 | 56.000 | 54.381 | 1.169 |
| 26.005 | 30.915 | 300.1 | 450 | Circular | 56.000 | 54.381 | 1.169 | 56.000 | 54.278 | 1.272 |
| 26.006 | 4.319 | 300.0 | 450 | Circular | 56.000 | 54.278 | 1.272 | | 54.264 | 1.286 |
| 26.007 | 49.445 | 300.0 | 450 | Circular | 56.000 | 54.264 | 1.286 | | 54.099 | 1.451 |
| 26.008 | 31.884 | 300.0 | 450 | Circular | 56.000 | 54.099 | 1.451 | | 53.993 | 2.147 |
| 26.009 | 33.969 | 300.0 | 450 | Circular | 56.590 | 53.993 | 2.147 | 56.820 | 53.880 | 2.490 |
| | Link | US | Dia | Node | мн | DS | Dia | Node | МН | |
| | | Node | (mm) | Туре | Туре | | • • | Туре | Туре | |
| | 24.000 | 76 | 1200 | Manhole | Adopta | | 1350 | Manhole | Adoptabl | е |
| | 23.001 | 77 | 1350 | Manhole | Adopta | ble 78 | 1350 | Manhole | Adoptabl | е |

| | Node | (mm) | Туре | Туре | Node | (mm) | Туре | Туре |
|--------|------|------|---------|-----------|------|------|---------|-----------|
| 24.000 | 76 | 1200 | Manhole | Adoptable | 77 | 1350 | Manhole | Adoptable |
| 23.001 | 77 | 1350 | Manhole | Adoptable | 78 | 1350 | Manhole | Adoptable |
| 23.002 | 78 | 1350 | Manhole | Adoptable | 79 | 1350 | Manhole | Adoptable |
| 23.003 | 79 | 1350 | Manhole | Adoptable | 80 | 1350 | Manhole | Adoptable |
| 19.009 | 80 | 1350 | Manhole | Adoptable | 83 | 1350 | Manhole | Adoptable |
| 25.000 | 81 | 1200 | Manhole | Adoptable | 82 | 1200 | Manhole | Adoptable |
| 25.001 | 82 | 1200 | Manhole | Adoptable | 83 | 1350 | Manhole | Adoptable |
| 19.010 | 83 | 1350 | Manhole | Adoptable | 84 | 1800 | Manhole | Adoptable |
| 1.015 | 84 | 1800 | Manhole | Adoptable | 85 | 1200 | Manhole | Adoptable |
| 1.016 | 85 | 1200 | Manhole | Adoptable | 86 | 1200 | Manhole | Adoptable |
| 1.017 | 86 | 1200 | Manhole | Adoptable | 87 | 1200 | Manhole | Adoptable |
| 1.018 | 87 | 1200 | Manhole | Adoptable | 88 | 1200 | Manhole | Adoptable |
| 1.019 | 88 | 1200 | Manhole | Adoptable | 107 | 1200 | Manhole | Adoptable |
| 26.000 | 89 | 1200 | Manhole | Adoptable | 90 | 1200 | Manhole | Adoptable |
| 26.001 | 90 | 1200 | Manhole | Adoptable | 92 | 1200 | Manhole | Adoptable |
| 27.000 | 91 | 1200 | Manhole | Adoptable | 92 | 1200 | Manhole | Adoptable |
| 26.002 | 92 | 1200 | Manhole | Adoptable | 93 | 1200 | Manhole | Adoptable |
| 26.003 | 93 | 1200 | Manhole | Adoptable | 95 | 1200 | Manhole | Adoptable |
| 28.000 | 94 | 1200 | Manhole | Adoptable | 95 | 1200 | Manhole | Adoptable |
| 26.004 | 95 | 1200 | Manhole | Adoptable | 96 | 1200 | Manhole | Adoptable |
| 26.005 | 96 | 1200 | Manhole | Adoptable | 97 | 1200 | Manhole | Adoptable |
| 26.006 | 97 | 1200 | Manhole | Adoptable | 98 | 1200 | Manhole | Adoptable |
| 26.007 | 98 | 1200 | Manhole | Adoptable | 99 | 1200 | Manhole | Adoptable |
| 26.008 | 99 | 1200 | Manhole | Adoptable | 100 | 1200 | Manhole | Adoptable |
| 26.009 | 100 | 1200 | Manhole | Adoptable | 102 | 1200 | Manhole | Adoptable |
| | | | | | | | | |

| CAUSEW | | Waterman Moylan Consulting | | | | 10-SW-NETV SW NETWO oghue 23 | • | Page 12 | | |
|--------|---------------|----------------------------|-------------------|-------------------------|-------------------------|---------------------------------------|-----------------------|-------------------------|---------------------|-----------------|
| | | | | | <u>Pipeline S</u> | <u>chedule</u> | | | | |
| Link | Length (m) | Slope (1:X) | Dia (mm) | Link Type | US CL (m) | US IL (m) | US Depth (m) | DS CL (m) | DS IL (m) | DS Depth (m) |
| 29.000 | 98.766 | 30.0 | 225 | Circular | 59.200 | 57.775 | 1.200 | 56.820 | 54.483 | 2.112 |
| 26.010 | 5.644 | 300.0 | 525 | Circular | 56.820 | 53.805 | 2.490 | 56.000 | 53.786 | 1.689 |
| 30.000 | 57.308 | 150.0 | 225 | Circular | 56.000 | 54.875 | 0.900 | 56.550 | 54.493 | 1.832 |
| 30.001 | 21.225 | 150.0 | 225 | Circular | 56.550 | 54.493 | 1.832 | 56.000 | 54.352 | 1.423 |
| 26.011 | 4.776 | 300.0 | 525 | Circular | 56.000 | 53.786 | 1.689 | 56.740 | 53.770 | 2.445 |
| 26.012 | 12.416 | 300.0 | 525 | Circular | 56.740 | 53.770 | 2.445 | 56.600 | 53.729 | 2.346 |
| 1.020 | 19.717 | 300.0 | 300 | Circular | 56.600 | 53.645 | 2.655 | 56.000 | 53.579 | 2.121 |
| | | ode (n | Dia nm) 200 | Node Type Manhole | MH Type Adoptable | DS Node 102 | Dia e (mm) 1200 | Node Type Manhole | MH Typ Adopta | e |

| | Node | (mm) | туре | туре | Node | (mm) | туре | туре | |
|--------|------|------|---------|-----------|---------|------|---------|-----------|--|
| 29.000 | 101 | 1200 | Manhole | Adoptable | 102 | 1200 | Manhole | Adoptable | |
| 26.010 | 102 | 1200 | Manhole | Adoptable | 105 | 1500 | Manhole | Adoptable | |
| 30.000 | 103 | 1200 | Manhole | Adoptable | 104 | 1200 | Manhole | Adoptable | |
| 30.001 | 104 | 1200 | Manhole | Adoptable | 105 | 1500 | Manhole | Adoptable | |
| 26.011 | 105 | 1500 | Manhole | Adoptable | 106 | 1200 | Manhole | Adoptable | |
| 26.012 | 106 | 1200 | Manhole | Adoptable | 107 | 1200 | Manhole | Adoptable | |
| 1.020 | 107 | 1200 | Manhole | Adoptable | 107_OUT | 1200 | Manhole | Adoptable | |
| | | | | | | | | | |

| Node | Easting (m) | Northing (m) | CL (m) | Depth (m) | Dia (mm) | Connections | Link | IL (m) | Dia (mm) |
|------|----------------|-----------------|-----------|--------------|-------------|-----------------------------|-------|-----------|-------------|
| 1 | 707582.615 | 733130.913 | 57.320 | 1.120 | 1200 | ✓ ^𝑘 | | | |
| | | | | | | 0 | 1.000 | 56.200 | 225 |
| 2 | 707631.554 | 733179.070 | 57.300 | 1.558 | 1200 | 1 | 1.000 | 55.742 | 225 |
| | | | | | | | 1.001 | 55.742 | 225 |
| 3 | 707646.088 | 733103.044 | 57.160 | 1.230 | 1200 | | | | |
| | | | | | | 0 | 2.000 | 55.930 | 225 |
| 4 | 707686.346 | 733143.264 | 56.800 | 1.535 | 1200 | 1 | 2.000 | 55.551 | 225 |
| | | | | | | 2 2 | 1.001 | 55.415 | 225 |
| | | | | | | ¹ ³ 0 | 1.002 | 55.265 | 375 |
| 5 | 707678.677 | 733040.140 | 56.680 | 1.240 | 1200 | () | | | |
| | | | | | | 0 | 3.000 | 55.440 | 225 |
| 6 | 707731.036 | 733092.449 | 56.180 | 1.253 | 1200 | 2. 1 | 3.000 | 55.070 | 225 |
| | | | | | | 2 | 1.002 | 54.927 | 375 |
| | | | | | | 1´ ^N 0 0 | 1.003 | 54.927 | 375 |
| 7 | 707766.868 | 733047.149 | 56.000 | 1.575 | 1350 | | 1.003 | 54.514 | 375 |
| | | | | | | • 0 | 1.004 | 54.425 | 450 |



| Node | Easting (m) | Northing (m) | CL (m) | Depth (m) | Dia (mm) | Connections | Link | IL (m) | Dia (mm) |
|------|----------------|-----------------|-----------|--------------|-------------|--|---------|------------------|-------------|
| 3 | 707795.011 | 733011.704 | 55.830 | 1.125 | 1200 | 0 | | | |
| | | | | | | | | | |
| | | | | | | 0 | 4.000 | 54.705 | 225 |
| 9 | 707776.870 | 733035.010 | 56.050 | 1.493 | 1200 | 1 | 4.000 | 54.557 | 225 |
| | | | | | | | | | |
| | | | | | | | 4.001 | 54.557 | 225 |
| 10 | 707767.760 | 733033.825 | 55.830 | 1.530 | 1200 | 2 1 | 4.001 | 54.511 | 225 |
| | | | | | | | 1.004 | 54.358 | 450 |
| | | | | | | | 1.005 | 54.200 | 450 |
| 11 | 707753.222 | 733019.219 | 56.020 | 1.864 | 1200 | 0 | 1.005 | 54.300 54.231 | 450 450 |
| | 101133.222 | 755015.215 | 50.020 | 1.004 | 1200 | | 1.005 | 54.251 | 450 |
| | | | | | | | | | |
| 12 | 707740.040 | 70007 640 | 56.000 | 4 700 | 4200 | 0 | 1.006 | 54.156 | 525 |
| 12 | 707748.849 | 733007.619 | 56.080 | 1.790 | 1200 | | | | |
| | | | | | | 0 ← () | | | |
| | | | | | | 0 | 5.000 | 54.290 | 225 |
| 13 | 707739.264 | 733008.337 | 56.170 | 2.100 | 1200 | 1 | 5.000 | 54.226 | 225 |
| | | | | | | | 1.006 | 54.097 | 525 |
| | | | | | | ° [∠] 0 | 1.007 | 54.070 | 525 |
| 14 | 707552.358 | 733030.718 | 57.220 | 1.450 | 1200 | | | | |
| | | | | | | \bigcirc | | | |
| | | | | | | 0 | 6.000 | 55.770 | 225 |
| 15 | 707580.419 | 732974.310 | 56.810 | 1.535 | 1200 | 1, 1 | 6.000 | 55.350 | 225 |
| | | | | | | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | | | |
| | | | | | | 0 | 6.001 | 55.275 | 300 |
| 16 | 707583.499 | 732975.911 | 56.900 | 1.814 | 1200 | . 1 | 6.001 | 55.236 | 300 |
| | | | | | | $\mathcal{A}^{\mathbf{p}}$ | | | |
| | | | | | | 1 | | | 450 |
| 17 | 707588.629 | 733018.388 | 56.900 | 1.500 | 1200 | 0 | 6.002 | 55.086 | 450 |
| ± / | 101500.025 | / 55010.500 | 50.500 | 1.500 | 1200 | \bigcirc | | | |
| | | | | | | \square | | | |
| 1.0 | 707607 207 | 732999.605 | 56.750 | 1 0 2 2 | 1200 | ° 0 | 7.000 | 55.400 | 225 |
| 18 | 707607.207 | /32999.005 | 50.750 | 1.832 | 1200 | | 6.002 | 55.106 54.918 | 225 450 |
| | | | | | | | | | |
| | | | | | | ² 0 | 6.003 | 54.918 | 375 |
| 19 | 707623.498 | 733015.910 | 56.550 | 1.799 | 1200 | 1 | 6.003 | 54.826 | 375 |
| | | | | | | \bigcirc | | | |
| | | | | | | 1 0 | 6.004 | 54.751 | 450 |
| 20 | 707557.536 | 733073.568 | 57.600 | 1.425 | 1200 | 70 | | | |
| | | | | | | \bigcirc | | | |
| | | | | | | 0 | 8.000 | 56.175 | 225 |
| | | | | | | , C | 1 - 200 | | 0 |



| Node | Easting (m) | Northing (m) | CL (m) | Depth (m) | Dia (mm) | Connections | Link | IL (m) | Dia (mm) |
|------|----------------|-----------------|-----------|--------------|-------------|-----------------------|----------------|------------------|-------------|
| 21 | 707582.693 | 733098.703 | 57.450 | 1.986 | 1200 | 1 | 8.000 | 55.464 | 225 |
| | | | | | | \bigcirc | | | |
| | | | | | | | 8.001 | 55.464 | 225 |
| 22 | 707639.436 | 733091.309 | 57.240 | 1.425 | 1200 | 0 | 0.001 | 55.404 | |
| | | | | | | \bigcirc | | | |
| | | | | | | | | | |
| 23 | 707614.894 | 733066.788 | 57.140 | 2.279 | 1200 | | 9.000 | 55.815 55.642 | 300 |
| 23 | 707014.004 | 755000.788 | 57.140 | 2.275 | 1200 | ² 2 | | 55.011 | 225 |
| | | | | | | X. | | | |
| 24 | 707655 260 | 700000 000 | 56.060 | 2 670 | 4200 | 0 | 8.002 | 54.861 | 375 |
| 24 | 707655.360 | 733026.683 | 56.860 | 2.670 | 1200 | | 8.002 6.004 | 54.576 54.639 | 375 450 |
| | | | | | | 2 2 2 | 0.004 | 54.055 | 430 |
| | | | | | | 0 | | 54.190 | 450 |
| 25 | 707667.633 | 733023.067 | 57.000 | 2.853 | 1200 | 1 | 6.005 | 54.147 | 450 |
| | | | | | | | | | |
| | | | | | | ÷ 0 | 6.006 | 54.155 | 450 |
| 26 | 707672.207 | 732986.631 | 55.150 | 1.117 | 1200 | 1 1 | 6.006 | 54.033 | 450 |
| | | | | | | $() \rightarrow_{0}$ | | | |
| | | | | | | 0 | 6.007 | 54.033 | 375 |
| 27 | 707691.305 | 732984.076 | 55.150 | 1.181 | 1200 | 1 | 6.007 | 53.969 | 375 |
| | | | | | | 1 | | | |
| | | | | | | | 6.000 | 52.000 | 450 |
| 28 | 707712.245 | 732992.966 | 57.000 | 1.925 | 1200 | 0 | 6.008 | 53.969 | 450 |
| 20 | /0//12.245 | 752552.500 | 37.000 | 1.525 | 1200 | \bigcirc | | | |
| | | | | | | \mathcal{Y} | | | |
| 20 | 707708.670 | 732977.575 | 55.150 | 1.243 | 1200 | 0 ⁰ 0 | | 55.075 | 225 225 |
| 29 | /0//08.0/0 | /329//.3/3 | 55.150 | 1.243 | 1200 | ² 2 2 | | 54.285 53.907 | 450 |
| | | | | | | ψ 3 | 1.007 | 53.925 | 525 |
| | | | | | | <mark>0</mark> 0 | 1.008 | 53.910 | 375 |
| 30 | 707590.871 | 732955.923 | 56.830 | 0.930 | 1200 | | | | |
| | | | | | | \bigcirc | | | |
| | | | | | | 0 و | 11.000 | 55.900 | 225 |
| 31 | 707627.313 | 732896.089 | 57.450 | 2.242 | 1200 | 1 1 | 11.000 | 55.433 | 225 |
| | | | | | | | | | |
| | | | | | | 0 | 11 001 | 55.208 | 450 |
| 32 | 707635.462 | 732901.380 | 57.600 | 2.441 | 1200 | 1 | | | 450 |
| | | | | | | \triangleleft | | | |
| | | | | | | | 11 002 | EE 150 | 150 |
| 33 | 707651.237 | 732917.100 | 57.050 | 2.336 | 1200 | 0 | | | 450 |
| | | | 27.000 | | 00 | | | 0 | .50 |
| | | | | | | | | | |
| | | | | | | 0 | 11.003 | 54.714 | 450 |



| Node | Easting (m) | Northing (m) | CL (m) | Depth (m) | Dia (mm) | Connections | Link | IL (m) | Dia (mm) |
|------|----------------|-----------------|-----------|--------------|-------------|------------------|------------------|-----------|-------------|
| 34 | 707638.572 | 732948.769 | 57.020 | 1.370 | 1200 | | | | |
| | | | | | | \bigcirc | | | |
| | | | | | | 0 | 12.000 | 55.650 | 225 |
| 35 | 707654.753 | 732932.519 | 56.830 | 1.295 | 1200 | 1 1 | 12.000 | 55.535 | 225 |
| | | | | | | →0 | | | |
| | | | | | | 0 | 12.001 | 55.535 | 225 |
| 36 | 707662.206 | 732933.154 | 56.860 | 2.431 | 1200 | 1 | 12.001 | 55.498 | 225 |
| | | | | | | 1 - 2 | 11.003 | 54.617 | 450 |
| 37 | 707647.642 | 733001.609 | 56.700 | 1.491 | 1200 | ² 0 | 11.004 | 54.429 | 525 |
| 57 | 707047.042 | /55001.005 | 50.700 | 1.491 | 1200 | \bigcirc | | | |
| | | | | | | 0 | 13.000 | 55.209 | 225 |
| 38 | 707689.219 | 732960.032 | 56.410 | 2.108 | 1200 | 1 | 13.000 | 54.493 | 225 |
| | | | | | | | 11.004 | 54.302 | 525 |
| | | | | | | 2 0 | 11.005 | 54.302 | 450 |
| 39 | 707709.094 | 732954.197 | 55.150 | 1.335 | 1200 | 2 0 | 11.005 11.005 | 54.302 | 450 |
| 00 | 1011001001 | , 0200 1127 | 551250 | 1.000 | 1200 | | 1.008 | 53.832 | 375 |
| | | | | | | 0 | 1.009 | 53.815 | 450 |
| 40 | 707809.077 | 732993.635 | 55.750 | 0.925 | 1200 | _ | | | |
| | | | | | | Q | | | |
| | | | | | | 0 | 14.000 | 54.825 | 225 |
| 41 | 707830.504 | 732966.107 | 55.750 | 1.425 | 1200 | 1 1 | 14.000 | 54.651 | 225 |
| | | | | | | \bigcirc | | | |
| | | | | | | 0 | 14.001 | 54.325 | 225 |
| 42 | 707830.561 | 732959.010 | 56.050 | 1.760 | 1200 | | 14.001 | 54.290 | 225 |
| | | | | | | \mathcal{Q} | | | |
| | | | | | | ° ² 0 | 14.002 | 54.290 | 225 |
| 43 | 707808.187 | 732936.671 | 56.060 | 1.928 | 1200 | 1 1 | 14.002 | 54.132 | 225 |
| | | | | | | \bigotimes | | | |
| | | | | | | 0 0 | 14.003 | 54.132 | 225 |
| 44 | 707793.010 | 732925.360 | 56.240 | 2.278 | 1200 | 1 | 14.003 | 54.037 | 225 |
| | | | | | | \boxtimes | | | |
| | | | | | | 0 0 | 14.004 | 53.962 | 300 |
| 45 | 707773.973 | 732906.324 | 56.630 | 2.776 | 1200 | ° 1 1 | 14.004 | 53.854 | 300 |
| | | | | | | | | | |
| | | | | | | 0 | 14.005 | 53.854 | 300 |
| 46 | 707731.229 | 732948.695 | 56.400 | 2.787 | 1200 | 1 | 14.005 | 53.613 | 300 |
| | | | | | | 0 < | | | |
| | | | | | | | 14.006 | 53.613 | 300 |
| | | | | | | Ŭ | 1 | | 201 |



| Node | Easting (m) | Northing (m) | CL (m) | Depth (m) | Dia (mm) | Connections | Link | IL (m) | Dia (mm) |
|------|----------------|-----------------|-----------|--------------|-------------|--------------------|--------|-----------|-------------|
| 47 | 707726.510 | 732973.051 | 56.300 | 1.425 | 1200 | | | . , | |
| | | | | | | \bigcirc | | | |
| | | | | | | ۰ O | 15.000 | 54.875 | 225 |
| 48 | 707725.039 | 732949.075 | 56.450 | 2.862 | 1200 | 1 1 | 15.000 | 54.395 | 225 |
| | | | | | | 2 2 | 14.006 | 53.588 | 300 |
| | | | | | | ° ² 0 | 14.007 | 53.839 | 375 |
| 49 | 707719.676 | 732942.481 | 56.570 | 2.808 | 1500 | ² 1 1 | 14.007 | 53.805 | 375 |
| | | | | | | 2 | 1.009 | 53.762 | 450 |
| 50 | 707667 200 | 722020 400 | 56.790 | 1.425 | 1200 | ° 0 | 1.010 | 53.770 | 450 |
| 50 | 707667.288 | 732838.488 | 56.790 | 1.425 | 1200 | ° | | | |
| | | | | | | 0 | 16.000 | 55.365 | 225 |
| 51 | 707633.852 | 732886.667 | 57.200 | 2.128 | 1200 | | 16.000 | 55.072 | 225 |
| | | | | | | | 16.001 | 55.072 | 225 |
| 52 | 707690.123 | 732872.909 | 56.690 | 1.540 | 1200 | 0 | | | |
| | | | | | | 0 | 17.000 | 55.150 | 225 |
| 53 | 707655.169 | 732907.984 | 57.030 | 2.234 | 1200 | 1 | 17.000 | 54.902 | 225 |
| | | | | | | 2 | 16.001 | 54.871 | 225 |
| | | | | | | 2 1 0 | 16.002 | 54.796 | 300 |
| 54 | 707697.549 | 732950.364 | 56.600 | 2.004 | 1200 | | 16.002 | 54.596 | 300 |
| | | | | | | 1 ¹ 000 | 16.003 | 54.596 | 300 |
| 55 | 707747.278 | 732900.622 | 56.700 | 1.425 | 1200 | • | | | |
| | | | | | | 0 | 18.000 | 55.275 | 225 |
| 56 | 707715.184 | 732932.724 | 56.700 | 2.262 | 1200 | 2 p 1 | 18.000 | 55.048 | 225 |
| | | | | | | 2 | 16.003 | 54.513 | 300 |
| | | | | | | ¹ 0 | 16.004 | 54.438 | 375 |
| 57 | 707722.058 | 732940.127 | 56.720 | 2.961 | 1200 | 2 1 | 16.004 | 54.387 | 375 |
| | | | | | | 2 | 1.010 | 53.759 | 450 |
| | | | | | | 1 ^{´ 0} 0 | 1.011 | 53.760 | 450 |
| 58 | 707731.855 | 732931.029 | 55.740 | 2.025 | 1200 | | 1.011 | 53.715 | 450 |
| | | | | | | 0 | 1.012 | 54.825 | 375 |
| 59 | 707758.967 | 732903.921 | 55.750 | 1.065 | 1200 | | 1.012 | 54.697 | 375 |
| | | | | | | 0 | 1.013 | 54.685 | 450 |
| | | | | | | 0 | 1.013 | 54 | .685 |



| Node | Easting (m) | Northing (m) | CL (m) | Depth (m) | Dia (mm) | Connections | 5 | Link | IL (m) | Dia (mm) |
|------|----------------|-----------------|-----------|--------------|-------------|--|---|------------------|------------------|-------------|
| 60 | 707765.933 | 732896.955 | 56.900 | 2.300 | 1350 | 1 0 | 1 | 1.013 | 54.652 | 450 |
| | | | | | | | | | | |
| | | | | | | | 0 | 1.014 | 54.600 | 450 |
| 61 | 707734.942 | 732764.697 | 57.410 | 1.425 | 1200 | _0_ | | | | |
| | | | | | | \bigtriangleup | | | | |
| | | | | | | \bigcirc | 0 | 10.000 | | 225 |
| 62 | 707770.349 | 732800.111 | 57.400 | 1.230 | 1200 | | 0 | 19.000 | 55.985 | 225 |
| 02 | /0///0.345 | ,52000.111 | 57.400 | 1.250 | 1200 | \bigcirc | | | | |
| | | | | | | \mathcal{L} | | | | |
| | | | | | | 0 | 0 | 20.000 | 56.170 | 225 |
| 63 | 707754.555 | 732784.314 | 57.610 | 1.839 | 1200 | ° 5 – 1 | 1 | 20.000 | 55.771 | 225 |
| | | | | | | \bigotimes | 2 | 19.000 | 55.846 | 225 |
| | | | | | | 2 | 0 | 19.001 | 55.771 | 225 |
| 64 | 707733.946 | 732804.922 | 57.170 | 1.863 | 1200 | 0 个 | 1 | 19.001 | 55.382 | 225 |
| | | | | | | ϕ | | | | |
| | | | | | | | 0 | 10.002 | FF 207 | 200 |
| 65 | 707731.572 | 732816.684 | 57.180 | 1.933 | 1200 | | 0 | 19.002 19.002 | 55.307 55.247 | 300 300 |
| 00 | ,0,,31.3,2 | /52010.004 | 57.100 | 1.555 | 1200 | ° | - | 10.002 | 55.247 | 500 |
| | | | | | | φ | | | | |
| | | | | | | 1 | 0 | 19.003 | 55.247 | 300 |
| 66 | 707713.370 | 732772.930 | 57.110 | 1.400 | 1200 | ° < | | | | |
| | | | | | | \bigcirc | | | | |
| | | | | | | | 0 | 21.000 | 55.710 | 225 |
| 67 | 707679.556 | 732820.801 | 56.800 | 1.556 | 1200 | 0 | 1 | 21.000 | 55.319 | 225 |
| | | | | | | $\overline{\mathbf{A}}$ | | | | |
| | | | | | | | 0 | 21.001 | EE 244 | 300 |
| 68 | 707703.518 | 732844.753 | 56.750 | 1.776 | 1200 | 0 | 0 | 21.001 21.001 | 55.244 55.075 | 300 |
| | | | | | | Å | 2 | 19.003 | 55.049 | 300 |
| | | | | | | | | | | |
| | | | | | | 1 2 | 0 | 19.004 | 54.974 | 375 |
| 69 | 707715.962 | 732866.502 | 56.800 | 1.951 | 1200 | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | 1 | 19.004 | 54.849 | 375 |
| | | | | | | \oslash | | | | |
| | | | | | | 1 | 0 | 19.005 | 54.849 | 375 |
| 70 | 707729.757 | 732880.144 | 56.800 | 2.091 | 1200 | | 1 | 19.005 | 54.784 | 375 |
| | | | | | | | | | | |
| | | | | | | 1 | 0 | 19.006 | E 4 700 | 450 |
| 71 | 707785.360 | 732827.871 | 57.100 | 1.425 | 1200 | 0 | 0 | 19.006 | 54.709 | 450 |
| - | | | 27.100 | | | ľ | | | | |
| | | | | | | \bigcirc | | | | |
| | | | | | | | 0 | 22.000 | 55.675 | 225 |
| 72 | 707775.426 | 732843.654 | 57.100 | 1.611 | 1200 | ° < | 1 | 22.000 | 55.489 | 225 |
| | | | | | | \bigotimes | | | | |
| | | | | | | 1 | 0 | 22.001 | 55.489 | 225 |
| | | | | | I | | | | | |



| Node | Easting (m) | Northing (m) | CL (m) | Depth (m) | Dia (mm) | Connections | Link | IL (m) | Dia (mm) |
|------|----------------|-----------------|-----------|--------------|-------------|--------------|-----------------|------------------|-------------|
| 73 | 707740.545 | 732878.534 | 56.700 | 2.027 | 1200 | | 1 22.001 | 54.996 | 225 |
| | | | | | | 2 | 2 19.006 | 54.673 | 450 |
| | | | | | | 1 |) 19.007 | 54.673 | 450 |
| 74 | 707749.441 | 732887.430 | 56.700 | 2.069 | 1350 | | 1 19.007 | 54.631 | 450 |
| | | | | | | 1 | 0 19.008 | 54.631 | 450 |
| 75 | 707859.264 | 732852.421 | 56.520 | 1.430 | 1200 | \bigcirc | | | |
| | | | | | | 0 | 0 23.000 | 55.090 | 300 |
| 76 | 707804.877 | 732798.070 | 57.020 | 1.250 | 1200 | \checkmark | | | |
| | | | | | | | 0 24.000 | 55.770 | 225 |
| 77 | 707829.427 | 732822.604 | 57.620 | 2.750 | 1350 | 0, 2 | 124.000223.000 | 55.596 54.879 | 225 300 |
| | | | | | | 1 | 0 23.001 | 54.870 | 375 |
| 78 | 707791.921 | 732860.029 | 57.000 | 2.370 | 1350 | 0 < | 1 23.001 | 54.693 | 375 |
| | | | | | | | 0 23.002 | 54.630 | 375 |
| 79 | 707779.375 | 732862.434 | 56.000 | 1.413 | 1350 | | 1 23.002 | 54.587 | 375 |
| | | | | | | | | | |
| | | | | | | |) 23.003 | 54.587 | 375 |
| 80 | 707766.010 | 732884.373 | 56.000 | 1.574 | 1350 | 7 | 1 23.003 | 54.501 | 375 |
| | | | | | | $\neg q$ | 2 19.008 | 54.575 | 450 |
| 81 | 707824.072 | 732839.343 | 57.000 | 1.125 | 1200 | 1 |) 19.009 | 54.426 | 450 |
| 01 | 101024.072 | 752035.343 | 57.000 | 1.125 | 1200 | ° | | | |
| | | | | | | | 25.000 | 55.875 | 225 |
| 82 | 707793.051 | 732870.402 | 57.000 | 2.003 | 1200 | • | 1 25.000 | 54.997 | 225 |
| | | | | | | | 0 25.001 | 54.997 | 225 |
| 83 | 707777.022 | 732896.708 | 56.860 | 2.595 | 1350 | | 1 25.001 | 54.843 | 225 |
| | | | | | | \square | 2 19.009 | 54.371 | 450 |
| | | | | | | |) 19.010 | 54.265 | 450 |
| 84 | 707777.981 | 732907.503 | 56.580 | 2.370 | 1800 | 70 | 1 19.010 | 54.229 | 450 |
| | | | | | | 2 | 2 1.014 | 54.210 | 450 |
| | 707707 655 | 70007 400 | FC 345 | 2 4 2 2 | 4000 | | 0 1.015 | 54.210 | 300 |
| 85 | 707797.658 | 732927.180 | 56.240 | 2.130 | 1200 | | 1 1.015 | 54.117 | 300 |
| | | | | | | 1 | 0 1.016 | 54.110 | 300 |



| Node | Easting (m) | Northing (m) | CL (m) | Depth (m) | Dia (mm) | Connections | Link | IL (m) | Dia (mm) |
|------|----------------|-----------------|-----------|--------------|-------------|---------------|---------------------------------|------------------|-------------|
| 86 | 707807.268 | 732934.340 | 56.020 | 1.950 | 1200 | 0 | 1 1.016 | 54.070 | 300 |
| | | | | | | | | | |
| | | | | | | | 1.017 | 54.070 | 300 |
| 87 | 707834.498 | 732961.081 | 56.900 | 2.957 | 1200 | | 1 1.017 | 53.943 | 300 |
| | | | | | | | | | |
| | | | | | | |) 1.018 | 53.943 | 300 |
| 88 | 707841.014 | 732964.358 | 55.630 | 1.711 | 1200 | | 1 1.018 | 53.919 | 300 |
| | | | | | | | 0 1.019 | 53.919 | 300 |
| 89 | 707813.378 | 732773.344 | 57.380 | 1.425 | 1200 | | | | |
| | | | | | | \bigcirc | | | |
| | | | | | | Ţ. | | | 2.25 |
| 90 | 707816.530 | 732753.705 | 57.900 | 2.044 | 1200 | | D26.000L26.000 | 55.955 55.856 | 225 |
| 50 | 707810.550 | 752755.705 | 57.900 | 2.044 | 1200 | → 0 | 20.000 | 55.850 | 22. |
| | | | | | | | 26.001 | 55.856 | 225 |
| 91 | 707874.700 | 732763.043 | 58.850 | 1.425 | 1200 | | | | |
| | | | | | | ₀ ← ⊖ | | | |
| | 707040 600 | 700750.000 | | 0 0 | 4000 | | 0 27.000 | 57.425 | 225 |
| 92 | 707849.689 | 732759.028 | 58.240 | 2.552 | 1200 | 1. | 1 27.000 2 26.001 | 56.792 55.688 | 225 225 |
| | | | | | | | 26.002 | 55.688 | 225 |
| 93 | 707845.749 | 732783.568 | 57.840 | 2.330 | 1200 | | 1 26.002 | 55.510 | 225 |
| | | | | | | φ^{*} | | | |
| | | | 56.000 | | 4000 | 1 (| 26.003 | 55.510 | 225 |
| 94 | 707885.570 | 732824.307 | 56.000 | 0.430 | 1200 | | | | |
| | | | | | | 04 | 28.000 | 55.570 | 225 |
| 95 | 707873.258 | 732811.989 | 56.000 | 1.530 | 1200 | 1 | 1 28.000 | 55.483 | 225 |
| | | | | | | | 2 26.003 | 55.114 | 225 |
| | | | | | | | 0 26.004 | 54.470 | 450 |
| 96 | 707892.179 | 732793.068 | 56.000 | 1.619 | 1200 | | 1 26.004 | 54.381 | 450 |
| | | | | | | | 26.005 | 54.381 | 450 |
| 97 | 707922.702 | 732797.973 | 56.000 | 1.722 | 1200 | | 1 26.005 | 54.278 | 450 |
| | | | | | | 1-07 | | | |
| | | | | | | l | 26.006 | 54.278 | 45(|
| 98 | 707925.756 | 732801.027 | 56.000 | 1.736 | 1200 | | 1 26.006 | 54.264 | 45(|
| | | | | | | 1 1 | 26.007 | 54.264 | 45(|
| | | | | | | 1 | 20.007 | 5-1.204 | -101 |



30

120

240

480

720

Manhole Schedule

| Node | Easting (m) | Northing (m) | CL (m) | Depth (m) | Dia (mm) | Connectio | ns | Link | IL (m) | Dia (mm) |
|----------|----------------|----------------------------|------------|--------------|-----------------|-----------------------------------|--------|--------|-----------|-------------|
| 99 | 707890.793 | 732835.990 | 56.000 | 1.901 | 1200 | • | 1 | 26.007 | 54.099 | 450 |
| | | | | | | 1 | 0 | 26.008 | 54.099 | 450 |
| 100 | 707868.297 | 732858.585 | 56.590 | 2.597 | 1200 | (C) | 1 | 26.008 | 53.993 | 45(|
| 101 | 707962.141 | 732812.736 | 59.200 | 1.425 | 1200 | 1 | 0 | 26.009 | 53.993 | 450 |
| 101 | 707502.141 | / 52012.750 | 55.200 | 1.425 | 1200 | ° | | | | |
| | | | | | | | 0 | 29.000 | 57.775 | 22 |
| 102 | 707892.325 | 732882.596 | 56.820 | 3.015 | 1200 | 7 | 1 | 29.000 | 54.483 | 225 |
| | | | | | | | 2 | 26.009 | 53.880 | 450 |
| 102 | 707045 472 | 722016 215 | 56.000 | 1.125 | 1200 | - ' | 0 | 26.010 | 53.805 | 52 |
| 103 | 707845.472 | 732946.315 | 56.000 | 1.125 | 1200 | Q | | | | |
| | | | | | | 0 | 0 | 30.000 | 54.875 | 22 |
| 104 | 707881.315 | 732901.600 | 56.550 | 2.057 | 1200 | | 1 | 30.000 | 54.493 | 22 |
| | | | | | | 0 | 0 | 30.001 | 54.493 | 22 |
| 105 | 707896.317 | 732886.586 | 56.000 | 2.214 | 1500 | 10 | 1 | 30.001 | 54.352 | 225 |
| | | | | | | X | 2 | 26.010 | 53.786 | 525 |
| 100 | 707000 005 | 700000000 | | 0.070 | 1000 | 2 | 0 | 26.011 | 53.786 | 525 |
| 106 | 707899.695 | 732889.962 | 56.740 | 2.970 | 1200 | | 1 | 26.011 | 53.770 | 52 |
| | | | | | | 1 | 0 | 26.012 | 53.770 | 525 |
| 107 | 707892.284 | 732899.924 | 56.600 | 2.955 | 1200 | 2 | 1 | 26.012 | 53.729 | 525 |
| | | | | | | X | 2 | 1.019 | 53.645 | 300 |
| 107 0117 | | 722012 200 | FC 000 | 2.421 | 1200 | 1 | 0 | 1.020 | 53.645 | 300 |
| 107_OUT | 707907.707 | 732912.208 | 56.000 | 2.421 | 1200 | | 1 | 1.020 | 53.579 | 300 |
| | | | | | | | | | | |
| | | | <u>Sin</u> | nulation S | <u>Settings</u> | | | | | |
| | | SR Region Sco | otland and | l Ireland | | Analys Skip Stea | ady St | tate x | rmal | |
| | M5 | | .300 | | | rain Down Tim | | - | | |
| | C., | Ratio-R 0.3 mmer CV 0.7 | | | | litional Storage heck Discharg | | | U | |
| | | Vinter CV 0.7 | | | | neck Discharge | | | | |
| | | | St | torm Dur | ations | | | | | |
| | L5 60 | 180 360 | | 960 | | L60 4320 | | 7200 | 10080 | |

1440

2880

5760

8640

| CAUSEWAY 🛟 | Waterman Moy | lan Consulting | File: 22-010-SW Network: SW N Paul Donoghue 19/10/2023 | | Page 21 |
|--|--|------------------------------|--|---|------------------------------------|
| R | eturn Period Cli (years) 100 | imate Change (CC %) 20 | Additional Area (A %) 0 | Additional Flo (Q %) | w 0 |
| | No | de 49 Online H | ydro-Brake [®] Cont | <u>rol</u> | |
| Replaces Downst Invert Design I | Flap Valve √ ream Link √ Level (m) 53.77 Depth (m) 2.500 Flow (l/s) 11.8 | Min Ou | Objective Sump Available Product Number tlet Diameter (m) le Diameter (mm) | √ CTL-SHE-0135- 0.150 | upstream storage 1180-2500-1180 |
| | <u>No</u> | de 84 Online H | <u>ydro-Brake® Cont</u> | <u>rol</u> | |
| Replaces Downst Invert Design I | Flap Valve √ ream Link √ Level (m) 54.21 Depth (m) 2.000 Flow (l/s) 19.4 | Min Ou | Objective Sump Available Product Number tlet Diameter (m) le Diameter (mm) | √ CTL-SHE-0181- 0.225 | upstream storage 1940-2000-1940 |
| | Nod | le 106 Online H | lydro-Brake [®] Con | trol | |
| Replaces Downst Invert Design I | Flap Valve √ ream Link √ Level (m) 53.77 Depth (m) 2.000 Flow (l/s) 3.4 | Min Ou | Objective Sump Available Product Number tlet Diameter (m) le Diameter (mm) | √ CTL-SHE-0075- 0.100 | upstream storage 3400-2000-3400 |
| | Noc | le 26 Depth/Ar | ea Storage Struct | <u>ure</u> | |
| Base Inf Coefficien Side Inf Coefficien | | , | | Invert I Time to half emp | Level (m) 54.033 ty (mins) |
| (m) | Area Inf Area (m²) (m²) 198.0 0.0 | (m) (| m²) (m²) 198.0 0.0 | Depth Area (m) (m²) 1.201 0.0 | (m²) |
| | Noc | le 27 Depth/Ar | ea Storage Struct | <u>ure</u> | |
| Base Inf Coefficien Side Inf Coefficien | | | | Invert I Time to half emp | Level (m) 53.969 ty (mins) |
| Depth (m) 0.000 | Area Inf Area (m²) (m²) 105.0 0.0 | (m) (r | rea Inf Area n²) (m²) 05.0 0.0 | DepthArea(m)(m²)1.2010.0 | Inf Area (m²) 0.0 |
| | Noc | le 49 Depth/Ar | ea Storage Struct | <u>ure</u> | |
| Base Inf Coefficien Side Inf Coefficien | | | | Invert I Time to half emp | .evel (m) 53.762 ty (mins) |
| Depth (m) 0.000 | Area Inf Area (m ²) (m ²) 295.0 0.0 | (m) (r | rea Inf Area n²) (m²) 05.0 0.0 | Depth Area (m) (m²) 1.201 0.0 | Inf Area (m²) 0.0 |



Node 59 Depth/Area Storage Structure

| Base Inf Coefficie Side Inf Coefficie | • • | • | | ty Factor Porosity | | Time to h | | ₋evel (m) ty (mins) | 54.685 |
|--|--------------|------------------|--------------|-----------------------|------------------|--------------|--------------|------------------------|--------|
| Depth (m) | Area (m²) | Inf Area (m²) | Depth (m) | Area (m²) | Inf Area (m²) | Depth (m) | Area (m²) | Inf Area (m²) | |
| 0.000 | 429.0 | 0.0 | 0.550 | 429.0 | 0.0 | 0.551 | 0.0 | 0.0 | |

Node 78 Depth/Area Storage Structure

| Base Inf Coefficient (m/hr) | 0.00000 | Safety Factor | 2.0 | Invert Level (m) | 54.630 |
|-----------------------------|---------|---------------|------|---------------------------|--------|
| Side Inf Coefficient (m/hr) | 0.00000 | Porosity | 1.00 | Time to half empty (mins) | 120 |

| • | | Inf Area (m²) | • | | | · · | | |
|-------|-------|------------------|-------|-------|-----|-------|-----|-----|
| 0.000 | 250.0 | 0.0 | 1.600 | 250.0 | 0.0 | 1.601 | 0.0 | 0.0 |

Node 80 Depth/Area Storage Structure

| Base Inf Coefficient (m/hr) | 0.00000 | Safety Factor | 2.0 | Invert Level (m) | 54.426 |
|-----------------------------|---------|---------------|------|---------------------------|--------|
| Side Inf Coefficient (m/hr) | 0.00000 | Porosity | 1.00 | Time to half empty (mins) | |

| • | | Inf Area (m²) | • | | | · · | | |
|-------|-------|------------------|-------|-------|-----|-------|-----|-----|
| 0.000 | 665.0 | 0.0 | 0.250 | 665.0 | 0.0 | 0.251 | 0.0 | 0.0 |

Node 99 Depth/Area Storage Structure

| Base Inf Coefficient (m/hr) | 0.00000 | Safety Factor | 2.0 | Invert Level (m) | 54.099 |
|-----------------------------|---------|---------------|------|---------------------------|--------|
| Side Inf Coefficient (m/hr) | 0.00000 | Porosity | 1.00 | Time to half empty (mins) | |

| • | | Inf Area (m²) | | | | • | | |
|-------|-------|------------------|-------|-------|-----|-------|-----|-----|
| 0.000 | 680.0 | 0.0 | 1.650 | 680.0 | 0.0 | 1.651 | 0.0 | 0.0 |



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Results for 100 year +20% CC Critical Storm Duration. Lowest mass balance: 98.24%

| Node Event | US Node | Peak (mins) | Level (m) | Depth (m) | Inflow (I/s) | Node Vol (m³) | Flood (m³) | Status |
|------------------|------------|----------------|--------------|--------------|-----------------|------------------|---------------|------------|
| 15 minute winter | 1 | 11 | 57.320 | 1.120 | 40.6 | 3.0666 | 1.3030 | FLOOD |
| 15 minute winter | 2 | 11 | 57.221 | 1.479 | 70.5 | 3.4579 | 0.0000 | FLOOD RISK |
| 15 minute winter | 3 | 11 | 56.982 | 1.052 | 53.1 | 3.2081 | 0.0000 | FLOOD RISK |
| 15 minute winter | 4 | 11 | 56.580 | 1.315 | 143.3 | 3.9384 | 0.0000 | FLOOD RISK |
| 15 minute winter | 5 | 10 | 56.680 | 1.240 | 83.8 | 5.1224 | 5.1497 | FLOOD |
| 15 minute winter | 6 | 10 | 56.180 | 1.253 | 253.7 | 5.1373 | 9.4476 | FLOOD |
| 15 minute winter | 7 | 11 | 55.618 | 1.193 | 223.0 | 2.6169 | 0.0000 | SURCHARGED |
| 15 minute winter | 8 | 11 | 55.686 | 0.981 | 26.2 | 2.1208 | 0.0000 | FLOOD RISK |
| 15 minute winter | 9 | 11 | 55.621 | 1.064 | 44.3 | 2.0306 | 0.0000 | SURCHARGED |
| 15 minute winter | 10 | 11 | 55.521 | 1.221 | 277.5 | 2.3383 | 0.0000 | SURCHARGED |
| 15 minute winter | 11 | 11 | 55.298 | 1.142 | 299.0 | 2.0272 | 0.0000 | SURCHARGED |
| 60 minute winter | 12 | 39 | 55.250 | 0.960 | 13.4 | 1.6969 | 0.0000 | SURCHARGED |
| 60 minute winter | 13 | 39 | 55.246 | 1.176 | 247.9 | 2.4275 | 0.0000 | SURCHARGED |
| 30 minute winter | 14 | 13 | 57.220 | 1.450 | 291.3 | 18.1192 | 116.3607 | FLOOD |
| 15 minute summer | 15 | 9 | 56.763 | 1.488 | 80.9 | 3.2732 | 0.0000 | FLOOD RISK |
| 15 minute winter | 16 | 8 | 56.722 | 1.636 | 88.5 | 1.8499 | 0.0000 | FLOOD RISK |
| 15 minute winter | 17 | 8 | 56.757 | 1.357 | 26.6 | 1.8973 | 0.0000 | FLOOD RISK |
| 15 minute winter | 18 | 8 | 56.722 | 1.804 | 126.6 | 3.7151 | 0.0000 | FLOOD RISK |
| 15 minute winter | 19 | 8 | 56.550 | 1.799 | 546.3 | 18.9938 | 110.0247 | FLOOD |
| 15 minute winter | 20 | 10 | 57.476 | 1.301 | 41.4 | 1.8733 | 0.0000 | FLOOD RISK |
| 15 minute summer | 21 | 10 | 57.450 | 1.986 | 62.7 | 3.8469 | 0.2864 | FLOOD |
| 15 minute winter | 22 | 10 | 57.209 | 1.394 | 53.1 | 3.8847 | 0.0000 | FLOOD RISK |
| 15 minute winter | 23 | 10 | 57.117 | 2.256 | 188.2 | 6.7464 | 0.0000 | FLOOD RISK |
| 15 minute summer | 24 | 9 | 56.615 | 2.425 | 411.3 | 6.6481 | 0.0000 | FLOOD RISK |
| 15 minute winter | 25 | 8 | 56.526 | 2.379 | 448.4 | 2.6908 | 0.0000 | SURCHARGED |

| Link Event | US | Link | DS | Outflow | Velocity | Flow/Cap | Link | Discharge |
|------------------|------|-------|------|---------|----------|----------|----------|-----------|
| (Upstream Depth) | Node | | Node | (I/s) | (m/s) | | Vol (m³) | Vol (m³) |
| 15 minute winter | 1 | 1.000 | 2 | 30.1 | 0.854 | 0.710 | 2.7307 | |
| 15 minute winter | 2 | 1.001 | 4 | 50.0 | 1.257 | 1.365 | 2.6032 | |
| 15 minute winter | 3 | 2.000 | 4 | 41.8 | 1.159 | 0.987 | 2.2633 | |
| 15 minute winter | 4 | 1.002 | 6 | 141.6 | 1.284 | 1.003 | 7.4639 | |
| 15 minute winter | 5 | 3.000 | 6 | 42.8 | 1.076 | 1.169 | 2.9435 | |
| 15 minute winter | 6 | 1.003 | 7 | 196.0 | 1.777 | 1.160 | 6.3709 | |
| 15 minute winter | 7 | 1.004 | 10 | 217.3 | 1.372 | 0.953 | 2.1159 | |
| 15 minute winter | 8 | 4.000 | 9 | 22.0 | 0.603 | 0.600 | 1.1746 | |
| 15 minute winter | 9 | 4.001 | 10 | 43.9 | 1.104 | 1.200 | 0.3654 | |
| 15 minute winter | 10 | 1.005 | 11 | 272.5 | 1.720 | 1.466 | 3.2652 | |
| 15 minute winter | 11 | 1.006 | 13 | 294.9 | 1.365 | 1.058 | 3.8236 | |
| 60 minute winter | 12 | 5.000 | 13 | 11.9 | 0.680 | 0.282 | 0.3823 | |
| 60 minute winter | 13 | 1.007 | 29 | 246.3 | 1.140 | 0.884 | 9.3726 | |
| 30 minute winter | 14 | 6.000 | 15 | 80.2 | 2.017 | 1.895 | 2.5057 | |
| 15 minute summer | 15 | 6.001 | 16 | 92.3 | 1.598 | 0.783 | 0.2444 | |
| 15 minute winter | 16 | 6.002 | 18 | 104.5 | 0.999 | 0.458 | 5.3107 | |
| 15 minute winter | 17 | 7.000 | 18 | -21.0 | 0.662 | -0.383 | 1.0507 | |
| 15 minute winter | 18 | 6.003 | 19 | 139.1 | 1.301 | 1.105 | 2.5422 | |
| 15 minute winter | 19 | 6.004 | 24 | 278.1 | 1.756 | 1.497 | 5.3291 | |
| 15 minute winter | 20 | 8.000 | 21 | -32.9 | -0.879 | -0.446 | 1.4143 | |
| 15 minute summer | 21 | 8.001 | 23 | 46.1 | 1.159 | 0.886 | 1.8031 | |
| 15 minute winter | 22 | 9.000 | 23 | 53.1 | 0.876 | 0.678 | 2.4431 | |
| 15 minute winter | 23 | 8.002 | 24 | 187.9 | 1.703 | 1.332 | 6.2840 | |
| 15 minute summer | 24 | 6.005 | 25 | 425.4 | 2.685 | 2.290 | 2.0273 | |
| 15 minute winter | 25 | 6.006 | 26 | 461.3 | 4.057 | 2.482 | 5.1273 | |
| | | | | | | | | |



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Results for 100 year +20% CC Critical Storm Duration. Lowest mass balance: 98.24%

| Node Event | US Node | Peak (mins) | Level (m) | Depth (m) | Inflow (I/s) | Node Vol (m³) | Flood (m³) | Status |
|--------------------------------|------------|----------------|--------------|--------------|-----------------|------------------------|--------------------|------------|
| 10080 minute winter | 26 | 4080 | 55.150 | 1.117 | 15.0 | 1339.4290 | 2097.4730 | FLOOD |
| 4320 minute winter | 27 | 1860 | 55.150 | 1.181 | 15.4 | 125.3407 | 13.1771 | FLOOD |
| 120 minute summer | 28 | 132 | 55.151 | 0.076 | 11.4 | 0.1305 | 0.0000 | ОК |
| 5760 minute winter | 29 | 2460 | 55.150 | 1.243 | 12.7 | 2.5457 | 899.9350 | FLOOD |
| 15 minute winter | 30 | 11 | 56.830 | 0.930 | 37.4 | 2.7119 | 0.9265 | FLOOD |
| 15 minute winter | 31 | 11 | 56.760 | 1.552 | 389.6 | 13.2747 | 0.0000 | SURCHARGED |
| 15 minute winter | 32 | 11 | 56.532 | 1.373 | 342.2 | 1.5529 | 0.0000 | SURCHARGED |
| 15 minute winter | 33 | 11 | 56.160 | 1.446 | 358.2 | 2.1298 | 0.0000 | SURCHARGED |
| 15 minute winter | 34 | 12 | 55.814 | 0.164 | 12.6 | 0.2530 | 0.0000 | ОК |
| 15 minute winter | 35 | 12 | 55.792 | 0.257 | 25.2 | 0.4016 | 0.0000 | SURCHARGED |
| 15 minute winter | 36 | 11 | 55.785 | 1.356 | 407.5 | 2.5379 | 0.0000 | SURCHARGED |
| 15 minute winter | 37 | 12 | 55.530 | 0.321 | 24.4 | 0.5957 | 0.0000 | SURCHARGED |
| 15 minute winter | 38 | 12 | 55.451 | 1.149 | 442.5 | 1.9649 | 0.0000 | SURCHARGED |
| 1440 minute winter | 39 | 690 | 55.150 | 1.335 | 34.9 | 1.5099 | 727.5891 | FLOOD |
| 15 minute winter | 40 | 12 | 55.579 | 0.754 | 26.2 | 1.7973 | 0.0000 | FLOOD RISK |
| 15 minute winter | 41 | 12 | 55.532 | 1.207 | 43.8 | 2.3472 | 0.0000 | FLOOD RISK |
| 15 minute winter | 42 | 12 | 55.479 | 1.189 | 45.4 | 1.7377 | 0.0000 | SURCHARGED |
| 60 minute winter | 43 | 38 | 55.437 | 1.305 | 32.2 | 1.8681 | 0.0000 | SURCHARGED |
| 60 minute winter | 44 | 38 | 55.342 | 1.380 | 40.8 | 2.1178 | 0.0000 | SURCHARGED |
| 60 minute winter | 45 | 39 | 55.299 | 1.445 | 51.8 | 2.2165 | 0.0000 | SURCHARGED |
| 60 minute summer | 46 | 39 | 55.283 | 1.670 | 75.4 | 2.5838 | 0.0000 | SURCHARGED |
| 60 minute winter | 47 | 38 | 55.296 | 0.421 | 13.6 | 0.8189 | 0.0000 | SURCHARGED |
| 60 minute summer | 48 | 39 | 55.242 | 1.654 | 90.1 | 1.8703 | 0.0000 | SURCHARGED |
| 60 minute winter | 49 | 38 | 55.206 | 1.444 | 323.8 | 356.6983 | 0.0000 | SURCHARGED |
| 15 minute winter | 50 | 12 | 56.757 | 1.392 | 35.2 | 3.0985 | 0.0000 | FLOOD RISK |
| Link Event (Upstream Depth) | US Node | Link | | | tflow V I/s) | /elocity Flov (m/s) | w/Cap Lir Vol (| ··· 0· |

| EIIIK EVCIIC | 05 | LIIIK | 0.5 | outilow | velocity | riow/cap | LIIIK | Discharge |
|---------------------|------|--------------|------|---------|----------|----------|----------|-----------|
| (Upstream Depth) | Node | | Node | (I/s) | (m/s) | | Vol (m³) | Vol (m³) |
| 10080 minute winter | 26 | 6.007 | 27 | 5.1 | 0.394 | 0.044 | 2.1252 | |
| 4320 minute winter | 27 | 6.008 | 29 | -15.4 | 0.223 | -0.083 | 2.9379 | |
| 120 minute summer | 28 | 10.000 | 29 | 11.4 | 1.352 | 0.097 | 0.4068 | |
| 5760 minute winter | 29 | 1.008 | 39 | 8.1 | 0.420 | 0.071 | 2.5790 | |
| 15 minute winter | 30 | 11.000 | 31 | 38.3 | 1.060 | 0.906 | 2.7863 | |
| 15 minute winter | 31 | 11.001 | 32 | 342.2 | 2.160 | 1.501 | 1.5394 | |
| 15 minute winter | 32 | 11.002 | 33 | 342.8 | 2.164 | 0.748 | 3.5285 | |
| 15 minute winter | 33 | 11.003 | 36 | 358.9 | 2.265 | 1.574 | 3.0808 | |
| 15 minute winter | 34 | 12.000 | 35 | 12.6 | 0.584 | 0.344 | 0.8121 | |
| 15 minute winter | 35 | 12.001 | 36 | 24.8 | 0.973 | 0.681 | 0.2975 | |
| 15 minute winter | 36 | 11.004 | 38 | 405.7 | 1.878 | 1.456 | 8.2324 | |
| 15 minute winter | 37 | 13.000 | 38 | 23.2 | 0.817 | 0.404 | 2.3385 | |
| 15 minute winter | 38 | 11.005 | 39 | 436.1 | 2.752 | 2.347 | 3.2820 | |
| 1440 minute winter | 39 | 1.009 | 49 | 13.3 | 0.917 | 0.071 | 2.5013 | |
| 15 minute winter | 40 | 14.000 | 41 | 18.3 | 0.895 | 0.501 | 1.3874 | |
| 15 minute winter | 41 | 14.001 | 42 | 34.7 | 0.873 | 0.948 | 0.2823 | |
| 15 minute winter | 42 | 14.002 | 43 | 43.5 | 1.094 | 1.189 | 1.2574 | |
| 60 minute winter | 43 | 14.003 | 44 | 30.9 | 0.876 | 0.844 | 0.7528 | |
| 60 minute winter | 44 | 14.004 | 45 | 39.4 | 0.639 | 0.563 | 1.8958 | |
| 60 minute winter | 45 | 14.005 | 46 | 50.1 | 0.712 | 0.717 | 4.2383 | |
| 60 minute summer | 46 | 14.006 | 48 | 73.2 | 1.040 | 1.046 | 0.4367 | |
| 60 minute winter | 47 | 15.000 | 48 | 30.3 | 1.331 | 0.411 | 0.9553 | |
| 60 minute summer | 48 | 14.007 | 49 | 86.9 | 0.788 | 0.690 | 0.9375 | |
| 60 minute winter | 49 | Hydro-Brake® | 57 | 4.2 | | | | |
| 15 minute winter | 50 | 16.000 | 51 | 25.9 | 0.760 | 0.709 | 2.3324 | |
| | | | | | | | | |



Results for 100 year +20% CC Critical Storm Duration. Lowest mass balance: 98.24%

| Node Event | US | Peak | Level | Depth | Inflow | Node | Flood | Status |
|-------------------|------|--------|--------|---------|----------|-----------------------|--------|--------------|
| | Node | (mins) | (m) | (m) | (I/s) | Vol (m ³) | (m³) | |
| 15 minute winter | 51 | 12 | 56.599 | 1.527 | 55.9 | 2.8471 | 0.0000 | SURCHARGED |
| 15 minute winter | 52 | 12 | 56.338 | 1.188 | 24.8 | 2.1913 | 0.0000 | SURCHARGED |
| 15 minute winter | 53 | 12 | 56.264 | 1.468 | 83.5 | 2.2919 | 0.0000 | SURCHARGED |
| 15 minute winter | 54 | 11 | 55.891 | 1.295 | 113.1 | 2.5623 | 0.0000 | SURCHARGED |
| 15 minute winter | 55 | 11 | 55.761 | 0.486 | 38.3 | 1.1293 | 0.0000 | SURCHARGED |
| 360 minute winter | 56 | 344 | 55.739 | 1.301 | 33.9 | 2.4498 | 0.0000 | SURCHARGED |
| 360 minute winter | 57 | 344 | 55.739 | 1.980 | 37.3 | 2.2393 | 0.0000 | SURCHARGED |
| 360 minute winter | 58 | 344 | 55.739 | 2.024 | 37.1 | 2.2890 | 0.0000 | FLOOD RISK |
| 360 minute winter | 59 | 344 | 55.739 | 1.054 | 63.4 | 237.3561 | 0.0000 | FLOOD RISK |
| 360 minute winter | 60 | 344 | 55.739 | 1.139 | 29.8 | 1.6293 | 0.0000 | SURCHARGED |
| 15 minute winter | 61 | 12 | 57.281 | 1.296 | 26.2 | 2.5198 | 0.0000 | FLOOD RISK |
| 15 minute winter | 62 | 12 | 57.322 | 1.152 | 41.9 | 3.0442 | 0.0000 | FLOOD RISK |
| 15 minute winter | 63 | 12 | 57.239 | 1.468 | 87.0 | 3.1443 | 0.0000 | SURCHARGED |
| 15 minute winter | 64 | 12 | 56.528 | 1.221 | 87.1 | 1.9457 | 0.0000 | SURCHARGED |
| 15 minute winter | 65 | 11 | 56.409 | 1.162 | 100.7 | 1.8311 | 0.0000 | SURCHARGED |
| 15 minute winter | 66 | 11 | 56.325 | 0.615 | 35.2 | 1.3813 | 0.0000 | SURCHARGED |
| 15 minute winter | 67 | 11 | 56.138 | 0.894 | 65.3 | 1.9077 | 0.0000 | SURCHARGED |
| 15 minute winter | 68 | 11 | 56.032 | 1.058 | 184.1 | 2.1624 | 0.0000 | SURCHARGED |
| 15 minute winter | 69 | 11 | 55.746 | 0.897 | 198.9 | 1.4103 | 0.0000 | SURCHARGED |
| 360 minute winter | 70 | 344 | 55.739 | 1.030 | 46.8 | 2.0033 | 0.0000 | SURCHARGED |
| 15 minute winter | 71 | 10 | 55.772 | 0.097 | 19.4 | 0.1684 | 0.0000 | ОК |
| 360 minute winter | 72 | 344 | 55.740 | 0.251 | 5.8 | 0.4171 | 0.0000 | SURCHARGED |
| 360 minute winter | 73 | 344 | 55.739 | 1.066 | 54.5 | 1.6583 | 0.0000 | SURCHARGED |
| 360 minute winter | 74 | 344 | 55.739 | 1.108 | 53.7 | 1.5859 | 0.0000 | SURCHARGED |
| 360 minute winter | 75 | 344 | 55.739 | 0.649 | 8.1 | 1.8150 | 0.0000 | SURCHARGED |
| Link Event | US | Link | DS | Outflow | Velocity | Flow/Ca | p Linl | c Discharge |
| (Upstream Depth) | Node | | Node | (I/s) | (m/s) | | Vol (r | n³) Vol (m³) |
| 15 minute winter | 51 | 16.001 | 53 | 50.1 | 1.260 |) 1.18 | 4 1.19 | 90 |
| 15 minute winter | 52 | 17.000 | 53 | 18.6 | 0.767 | 0.50 | 9 1.96 | 94 |
| 15 minute winter | 53 | 16.002 | 54 | 85.0 | 1.207 | / 1.33 | 2 4.22 | .05 |
| 15 minute winter | 54 | 16.003 | 56 | 112.4 | 1.596 | 5 1.76 | 2 1.75 | 65 |
| 15 minute winter | 55 | 18.000 | 56 | 33.8 | 0.985 | 0.92 | 2 1.80 | 53 |

| 15 minute winter | 53 | 16.002 | 54 | 85.0 | 1.207 | 1.332 | 4.2205 | |
|-------------------|----|--------|----|-------|-------|--------|--------|--|
| 15 minute winter | 54 | 16.003 | 56 | 112.4 | 1.596 | 1.762 | 1.7565 | |
| 15 minute winter | 55 | 18.000 | 56 | 33.8 | 0.985 | 0.922 | 1.8053 | |
| 360 minute winter | 56 | 16.004 | 57 | 33.8 | 0.569 | 0.240 | 1.1142 | |
| 360 minute winter | 57 | 1.011 | 58 | 37.1 | 0.234 | 0.200 | 2.1184 | |
| 360 minute winter | 58 | 1.012 | 59 | 36.1 | 0.884 | 0.314 | 4.2287 | |
| 360 minute winter | 59 | 1.013 | 60 | -29.0 | 0.732 | -0.156 | 1.5608 | |
| 360 minute winter | 60 | 1.014 | 84 | -29.8 | 0.196 | -0.059 | 2.5372 | |
| 15 minute winter | 61 | 19.000 | 63 | 19.4 | 0.787 | 0.531 | 1.1032 | |
| 15 minute winter | 62 | 20.000 | 63 | 34.1 | 1.005 | 0.490 | 0.8884 | |
| 15 minute winter | 63 | 19.001 | 64 | 75.0 | 1.886 | 1.248 | 1.1591 | |
| 15 minute winter | 64 | 19.002 | 65 | 89.5 | 1.272 | 1.143 | 0.8450 | |
| 15 minute winter | 65 | 19.003 | 68 | 103.9 | 1.475 | 1.327 | 2.7946 | |
| 15 minute winter | 66 | 21.000 | 67 | 30.1 | 1.067 | 0.711 | 2.3309 | |
| 15 minute winter | 67 | 21.001 | 68 | 55.3 | 0.909 | 0.707 | 2.3858 | |
| 15 minute winter | 68 | 19.004 | 69 | 185.1 | 1.678 | 1.312 | 2.7637 | |
| 15 minute winter | 69 | 19.005 | 70 | 199.9 | 1.813 | 1.739 | 2.1399 | |
| 360 minute winter | 70 | 19.006 | 73 | 45.8 | 0.721 | 0.247 | 1.7281 | |
| 15 minute winter | 71 | 22.000 | 72 | 19.4 | 0.901 | 0.374 | 0.4016 | |
| 360 minute winter | 72 | 22.001 | 73 | 5.9 | 0.867 | 0.113 | 1.9618 | |
| 360 minute winter | 73 | 19.007 | 74 | 53.7 | 0.859 | 0.289 | 1.9934 | |
| 360 minute winter | 74 | 19.008 | 80 | 52.7 | 0.935 | 0.284 | 2.6696 | |
| 360 minute winter | 75 | 23.000 | 77 | 8.1 | 0.579 | 0.103 | 2.9704 | |
| | | | | | | | | |



Results for 100 year +20% CC Critical Storm Duration. Lowest mass balance: 98.24%

| Node Event | US Node | Peak (mins) | Level (m) | Depth (m) | Inflow (I/s) | Node Vol (m³) | Flood (m³) | Status |
|--------------------|------------|----------------|--------------|--------------|-----------------|------------------|---------------|------------|
| 15 minute winter | 76 | 10 | 55.894 | 0.124 | 20.7 | 0.2319 | 0.0000 | ОК |
| 360 minute winter | 77 | 344 | 55.739 | 0.869 | 17.0 | 1.7821 | 0.0000 | SURCHARGED |
| 360 minute winter | 78 | 344 | 55.739 | 1.109 | 56.2 | 278.9014 | 0.0000 | SURCHARGED |
| 360 minute winter | 79 | 344 | 55.739 | 1.152 | 46.2 | 2.1385 | 0.0000 | FLOOD RISK |
| 360 minute winter | 80 | 344 | 55.739 | 1.313 | 63.0 | 168.9632 | 0.0000 | FLOOD RISK |
| 15 minute winter | 81 | 10 | 55.980 | 0.105 | 32.9 | 0.2541 | 0.0000 | ОК |
| 360 minute winter | 82 | 344 | 55.739 | 0.742 | 10.3 | 1.4175 | 0.0000 | SURCHARGED |
| 360 minute winter | 83 | 344 | 55.739 | 1.474 | 50.1 | 2.9963 | 0.0000 | SURCHARGED |
| 360 minute winter | 84 | 344 | 55.739 | 1.529 | 49.4 | 3.8901 | 0.0000 | SURCHARGED |
| 360 minute winter | 85 | 160 | 54.232 | 0.122 | 19.4 | 0.1377 | 0.0000 | ОК |
| 360 minute winter | 86 | 160 | 54.185 | 0.115 | 19.4 | 0.1298 | 0.0000 | ОК |
| 15 minute summer | 87 | 37 | 54.066 | 0.123 | 19.4 | 0.1396 | 0.0000 | ОК |
| 15 minute summer | 88 | 37 | 54.031 | 0.112 | 19.4 | 0.1266 | 0.0000 | ОК |
| 15 minute winter | 89 | 11 | 56.900 | 0.945 | 34.1 | 1.3999 | 0.0000 | SURCHARGED |
| 15 minute winter | 90 | 11 | 56.875 | 1.019 | 20.7 | 1.4027 | 0.0000 | SURCHARGED |
| 15 minute winter | 91 | 10 | 57.487 | 0.062 | 13.1 | 0.0955 | 0.0000 | ОК |
| 15 minute winter | 92 | 11 | 56.844 | 1.156 | 43.7 | 1.7151 | 0.0000 | SURCHARGED |
| 15 minute winter | 93 | 11 | 56.647 | 1.137 | 91.7 | 2.5348 | 0.0000 | SURCHARGED |
| 15 minute summer | 94 | 1 | 55.570 | 0.000 | 0.0 | 0.0000 | 0.0000 | ОК |
| 15 minute winter | 95 | 9 | 55.522 | 1.052 | 141.1 | 3.0180 | 0.0000 | SURCHARGED |
| 2880 minute winter | 96 | 2760 | 55.518 | 1.137 | 6.5 | 2.0306 | 0.0000 | SURCHARGED |
| 2880 minute winter | 97 | 2760 | 55.518 | 1.240 | 8.7 | 3.6491 | 0.0000 | SURCHARGED |
| 2880 minute winter | 98 | 2760 | 55.518 | 1.254 | 10.4 | 3.1223 | 0.0000 | SURCHARGED |
| 2880 minute winter | 99 | 2760 | 55.518 | 1.419 | 18.1 | 966.4634 | 0.0000 | SURCHARGED |
| 2880 minute winter | 100 | 2760 | 55.518 | 1.525 | 7.9 | 3.3456 | 0.0000 | SURCHARGED |

| (Upstream Depth) Node Node (I/s) (m/s) Vol (m ³) | Vol (m³) |
|---|----------|
| (Upstream Depth) Node Node (I/s) (m/s) Vol (m³) 15 minute winter 76 24.000 77 20.5 0.938 0.560 0.7588 | |
| 360 minute winter 77 23.001 78 16.5 0.731 0.143 5.8440 | |
| 360 minute winter 78 23.002 79 -47.4 -0.751 -0.412 1.4089 | |
| 360 minute winter 79 23.003 80 -44.8 0.588 -0.389 2.8334 | |
| 360 minute winter 80 19.009 83 34.6 0.633 0.186 2.6199 | |
| 15 minute winter 81 25.000 82 32.9 0.985 0.446 1.2693 | |
| 360 minute winter 82 25.000 82 52.5 0.565 0.440 1.2555 360 minute winter 82 25.001 83 10.3 0.779 0.280 1.2251 | |
| 360 minute winter 82 23.001 83 10.5 0.775 0.266 1.7251 360 minute winter 83 19.010 84 49.4 0.410 0.266 1.7172 | |
| 360 minute winter 84 Hydro-Brake [®] 85 19.4 | |
| 360 minute winter 85 1.016 86 19.4 0.751 0.304 0.3091 | |
| 360 minute winter 86 1.010 86 19.4 0.751 0.304 0.3051 360 minute winter 86 1.017 87 19.4 0.744 0.303 0.9934 | |
| 15 minute summer 87 1.018 88 19.4 1.008 0.304 0.1869 | |
| 15 minute summer 88 1.019 107 19.4 0.754 0.304 2.1255 | |
| 15 minute summer 88 1.019 107 19.4 0.754 0.504 2.1255 15 minute winter 89 26.000 90 -22.8 0.606 -0.622 0.7910 | |
| 15 minute winter 90 26.001 92 24.4 0.614 0.666 1.3357 | |
| | |
| 15 minute winter 91 27.000 92 13.1 1.502 0.159 0.2210 15 minute winter 02 26.002 03 45.5 1.144 1.038 0.0885 | |
| 15 minute winter 92 26.002 93 45.5 1.144 1.038 0.9885 15 minute winter 92 26.002 93 45.5 1.144 1.038 0.9885 | |
| 15 minute winter 93 26.003 95 89.9 2.261 1.730 1.5731 | |
| 15 minute summer 94 28.000 95 0.0 0.000 0.000 0.0273 | |
| 15 minute winter 95 26.004 96 149.7 0.945 0.806 4.2396 | |
| 2880 minute winter 96 26.005 97 6.4 0.378 0.035 4.8983 | |
| 2880 minute winter 97 26.006 98 8.6 0.439 0.047 0.6843 | |
| 2880 minute winter 98 26.007 99 10.4 0.582 0.056 7.8342 | |
| 2880 minute winter 99 26.008 100 -7.8 0.268 -0.042 5.0518 | |
| 2880 minute winter 100 26.009 102 -5.8 0.320 -0.031 5.3822 | |



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Results for 100 year +20% CC Critical Storm Duration. Lowest mass balance: 98.24%

| Node Event | US Node | Peak (mins) | Level (m) | Depth (m) | Inflow (I/s) | Node Vol (m³) | Flood (m³) | Status |
|--------------------|------------|----------------|--------------|--------------|-----------------|------------------|---------------|------------|
| 15 minute winter | 101 | 10 | 57.956 | 0.181 | 84.7 | 0.6810 | 0.0000 | ОК |
| 15 minute summer | 102 | 10 | 55.566 | 1.761 | 241.7 | 4.7595 | 0.0000 | SURCHARGED |
| 15 minute summer | 103 | 10 | 56.000 | 1.125 | 37.4 | 2.9329 | 1.1315 | FLOOD |
| 15 minute summer | 104 | 10 | 55.892 | 1.399 | 60.1 | 2.7110 | 0.0000 | SURCHARGED |
| 15 minute summer | 105 | 10 | 55.568 | 1.782 | 76.1 | 3.1482 | 0.0000 | SURCHARGED |
| 15 minute summer | 106 | 10 | 55.567 | 1.797 | 15.5 | 2.0326 | 0.0000 | SURCHARGED |
| 2880 minute winter | 107 | 2700 | 53.773 | 0.128 | 22.6 | 0.1447 | 0.0000 | ОК |
| 2880 minute winter | 107_OUT | 2700 | 53.693 | 0.114 | 22.6 | 0.0000 | 0.0000 | ОК |

| Link Event (Upstream Depth) | US Node | Link | DS Node | Outflow (I/s) | Velocity (m/s) | Flow/Cap | Link Vol (m³) | Discharge Vol (m ³) |
|--------------------------------|------------|--------------|------------|------------------|-------------------|----------|------------------|------------------------------------|
| 15 minute winter | 101 | 29.000 | 102 | 84.0 | 2.151 | 0.882 | 3.6516 | |
| 15 minute summer | 102 | 26.010 | 105 | -89.1 | 0.598 | -0.320 | 1.2193 | |
| 15 minute summer | 103 | 30.000 | 104 | 36.4 | 0.916 | 0.860 | 2.2792 | |
| 15 minute summer | 104 | 30.001 | 105 | 70.1 | 1.762 | 1.654 | 0.8441 | |
| 15 minute summer | 105 | 26.011 | 106 | 15.5 | 0.680 | 0.056 | 1.0318 | |
| 15 minute summer | 106 | Hydro-Brake® | 107 | 3.2 | | | | |
| 2880 minute winter | 107 | 1.020 | 107_OUT | 22.6 | 0.847 | 0.354 | 0.5254 | 3107.1 |

Surface Water Management Plan Project Number: 22-010 Document Reference: 22-010r.017 Surface Water Management Plan

UK and Ireland Office Locations

